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Patent Application
Docket No. CRX.106XC1
Serial No. 10/662,492

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

Examiner : Patrick Butler
Art Unit : 1732
Applicant : Albert E. Ortega
Serial No. : 10/662,492
Conf. No. : 9209
Filed : September 15, 2003
For : Method of Reducing Static in a Spunbond Process

Commissioner for Patents
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Alexandria, VA 22313-1450

EXPERT DECLARATION OF ALBERT E. ORTEGA UNDER 37 CFR §1.132

Sir:

I, Albert E. Ortega, hereby declare:

THAT, I have reviewed the above-referenced patent application, including the claims;

THAT, I have reviewed the Office Action dated August 6, 2010, along with the references cited therein;

THAT, I have extensive experience in the field of spunbond processes;

And being thus duly qualified, do further declare as follows:

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1. Using bicomponent fibers containing metal or carbon in a spunbond process is very expensive, plugs filters and packs, and changes the natural color of the fabric being produced. If metal or carbon were used as an antistatic agent in a spunbond process, as suggested at page 5 of the Action of August 6, 2010, the unintended consequence of changing the color would be considered by a skilled artisan as causing a defect in the spunbonded fabric. In addition, the high amount of metal and/or carbon that would be required to be added in order to reduce the static level measured at about one half inch below the outlet of the slot attenuation device from greater than 2 kilovolt per inch or less than -2 kilovolt per inch to between -2 kilovolt per inch and 2 kilovolt per inch would significantly change the natural color of the spunbonded fabric being produced.

2. I would understand from the original specification of the subject application (serial number 10/662,492) that the described method of producing a spunbonded nonwoven fabric, including the addition of an antistatic agent to the melt blend, does not cause any defects in the fabric. For example, the specification discloses on multiple occasions that the described method reduces fabric defects (e.g., page 3, lines 30-31).

3. The Action of August 6, 2010 states at page 2 that "Gillespie [U.S. Patent No. 5,783,503] teaches using combinations including nylon and polyester (see Gillespie, col. 4, lines 66 – col 5, line 25). Increases in moisture absorbency increase fiber conductivity, which is antistatic since it limits static buildup, and nylon's or polyester's presence would improve fiber conductivity, which is antistatic since it limits static buildup, and nylon's or polyester's presence would improve the absorbency of the blend since they have 0.4-4.5% standard moisture regain." This seems to imply that, as the nylon content (compared to the polyolefin content) increases, the static dissipation in a spunbond process should improve, such that a 100% nylon process would have dramatically improved static dissipation properties over a 100% polyolefin process. However, this is not the case. A slot spunbond polyolefin process does not generate near the static at the exit of an attenuation device that a nylon slot spunbond process does. Also, in the nylon process, the polymer exits the

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spinneret with little to no moisture since the moisture is removed by drying the resin or flashed off during spinning. One possible explanation for the fact that the presence of nylon does not reduce the static in practice is that the amount of time between the exit of the spinneret and the exit of the slot may not be sufficient for the nylon to absorb enough water to make an impact.

4. The Action of August 6, 2010 at pages 2-4 discusses spinning nylon along with polyolefins, referencing Gillespie and Tortora (*Understanding Textiles*). However, the melting point of polyolefin is much lower than nylon. Commonly used polyolefins melt around 160 to 170 °C where nylon 6 melts at 228 °C and nylon 6,6 at 269°C. Polyolefin fabric would completely melt if a bonding temperature of between 180 °C and about 250 °C were used. Also, the nylon spinning process would not allow the processing of polyolefins; it is just too hot. Gillespie makes this point in column 8, lines 40 -52, stating that “[t]he polymers should be selected to have melting temperatures and should be spun at a polymer throughput that enables the spinning of the components through a common capillary at substantially the same temperature without degrading one of the components. For example, nylon is typically extruded at a temperature of approximately 250 to 270 degrees Centigrade. Polyethylene and polypropylene typically are extruded at a temperature of approximately 200 to 230 degrees Centigrade. The polymers come together in the spin pack at the same capillary at a temperature of about 250 degrees Centigrade and are spun at a polymer throughput that avoids degradation of the lower melting component.” This point is also emphasized in U.S. Patent Application Publication No. 2003/0181112 which discloses a spunbonded nonwoven fabric which is made of a polyolefin resin. The melt point of the polyethylene resin is “in the range of 100 to 140 °C (page 4, paragraph [0061]). This emphasizes that a polyolefin fabric would completely melt, potentially destroying the spunbonding equipment, if a bonding temperature of between 180 °C and about 250 °C were used.

5. The Action of August 6, 2010 at page 5 states that “Gillespie does teach to incorporate into the polymer melt components to control electrical properties (forming in an extruder) (see col.5, lines

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35-42).” However, Gillespie’s comments regarding controlling electrical properties are not related to minimizing static issues but rather producing a splittable filament. Gillespie discloses that “[t]he properties of a single polymer can be manipulated by the addition of various modifiers to, in effect, create polymers of suitably different properties that do not adhere well to each other for use in the practice of the invention. For example, a single polymer can be used for first and second components with suitable additives to control the surface free energy, electrical properties or crystallization so as to produce a splittable filament” (column 5, lines 32-39). Gillespie does not discuss using an antistatic agent but instead discusses the use of additives to facilitate making a splittable fiber.

6. Gillespie teaches that “[a] triboelectric charge can be developed in the filaments to promote separation... [a] nylon component can develop such a static charge... (and) [a]n external electric field can be applied to the filaments... to augment the separation” (column 9, lines 53-63). Thus, addition to the melt blend, in the Gillespie process, of additives that would lower the static level at the outlet of an attenuation device would inhibit separation of the filaments, in direct contrast to the goal of the Gillespie process.

7. The Action of August 6, 2010 states at page 6 that “[i]t would have been obvious to one of ordinary skill in the art at the time of the invention to select nylon 6 as the nylon to use in Gillespie in order to have greater tenacity.” Although nylon 6 has greater yarn tenacity, it is not necessarily true that nylon 6 has greater fabric tenacity. Fabric tensile strength is a function of many things and is not limited to just yarn tenacity. The bond area of the calender, the calender temperature and pressure, and the line speed are just a few of the variables that impact fabric strength.

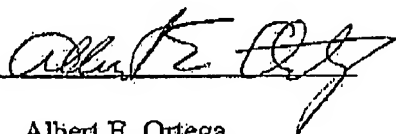
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I hereby further declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code, and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

By:



Albert E. Ortega

Date:

12-2-10

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(54) **SPUNBONDED NONWOVEN FABRIC AND
 ABSORBENT ARTICLE**

Publication Classification

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(57) **ABSTRACT**

(21) Appl. No.: **10/297,596**

(22) PCT Filed: **Jun. 13, 2001**

(86) PCT No.: **PCT/JP01/04984**

(30) **Foreign Application Priority Data**

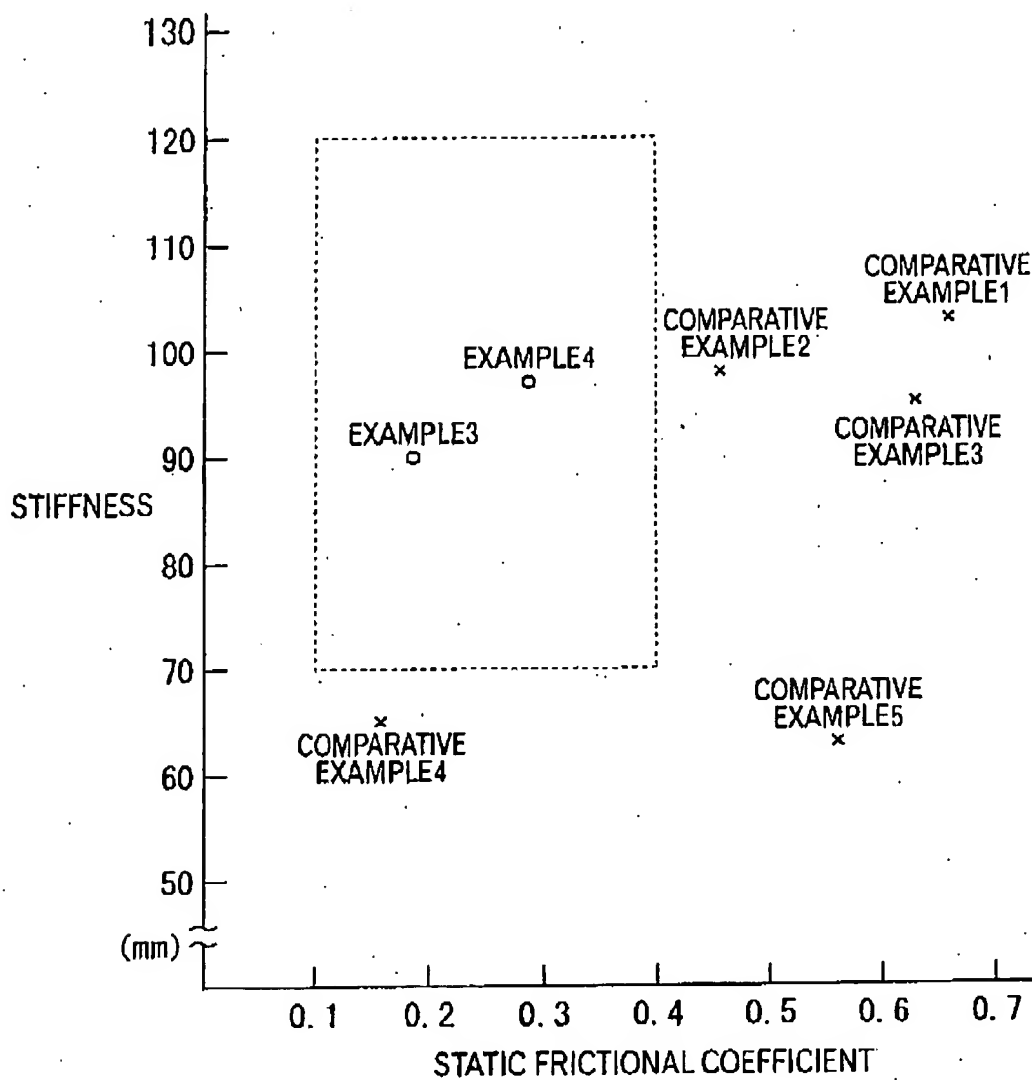
Jun. 13, 2000 (JP) **2000-176508**
 Jun. 23, 2000 (JP) **2000-188726**
 Jul. 26, 2000 (JP) **2000-225657**

A spunbonded nonwoven fabric which is made of a poly-
 olefin resin and has an average fiber diameter of 5 to 60 μm ,
 METSUE of 5 to 200 g/m^2 , and a coefficient of static
 friction of 0.1 to 0.4; or a spunbonded nonwoven fabric
 which is made of a polypropylene resin and has a stiffness
 [sum of the values for the longitudinal and transverse
 directions as obtained according to JIS L 1096, 6.19.1,
 method A (45° cantilever method)] of 70 to 120 mm and a
 coefficient of static friction of 0.1 to 0.4.

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FIG. 1



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SPUNBONDED NONWOVEN FABRIC AND ABSORBENT ARTICLE

TECHNICAL FIELD

[0001] The present invention relates to a nonwoven polyolefin resin fabric and an absorbent article used this. In particular, the present invention relates to a nonwoven fabric which has good flexibility, feeling and touch to the skin, and excellent strength, bending rigidity and post-processability, and is capable of using suitably as a material for absorbent article such as disposable diaper and the like.

BACKGROUND OF THE INVENTION

[0002] A nonwoven thermoplastic resin long fiber fabric has been used in many fields, since it has characteristics such as mechanical property like tensile strength, bending rigidity, gas permeability and the like, and at the same time it has excellent continuous spinability and productivity. The thermoplastic resins used to these nonwoven long fiber fabric have been used polyamide resins and polyester resins from melt spinability, fiber characteristic and the like, however polyolefin resins such as polypropylene, polyethylene and the like, which are general purpose resin, have been much used.

[0003] Among the nonwoven fabric comprising these polyolefin resins, for example, the polypropylene resin comprises many resins having different degree of crystallinity, even though in homopolymers of propylene, and also it is known that there are many resins having different crystallinity, and also resins having various characteristics such as melting point, strength, elastic modulus and the like by means of copolymers of propylene with ethylene, butene-1 or the like. The nonwoven fabric used such polypropylene resins has good spinability in the case of resin having high degree of crystallinity, however it has problem of poor flexibility and feeling. And moreover, in the case of polypropylene resins having low degree of crystallinity or low melting point, it has flexibility, however there are problems of slimy feeling, and large friction resistance between fibers, fiber and other metal and the like at the time of spinning, and become very worse in the spinability, or usage feeling is poor in articles contacting to the skin such as the absorbent article.

[0004] Further, in the case of resins having approximate 90 mol % of isotactic pentad fraction, there are problem that characteristics such as strength, rigidity or the like, and also spinability are relatively favorable, however in the case of used to absorbent articles such as disposable diaper, sanitary napkin, incontinent pad and the like, the obtained nonwoven fabric has not always sufficient using feel such as feeling, touch to the skin and the like.

[0005] Various improvements with the spunbonded nonwoven fabric composed of the polypropylene resin long fiber have been proposed. For example, (1) Japanese Patent Laid Open No. 13238/1996 disclosed polypropylene resin compositions for fiber containing crystalline polypropylene resins having ratio (Mw/Mn) of mass average molecular weight (Mw) to number average molecular weight (Mn) of 2 to 15, and isotactic pentad fraction of 96% or more of 100 mass parts, and fatty acid amide compounds of 0.01 to 1 mass parts.

[0006] This official gazette intends to improve poor drawing by fuzzing at the drawing time, by adding lubricants to improve drawability and luster in manufacturing of high strength fibers by high draw ratio of 6 times or more, used high crystalline polypropylene resins. That is, this proposal describes only that the resin differ from the range of crystallinity much used in nonwoven polypropylene resin fabrics, and it is not always favorable in flexibility, feeling and touch to the skin, and it is used suitably to industrial material such as nonwoven fabrics, and it is not nonwoven fabrics for the absorbent article, and it relates to fibers for special use which intended improvement of strength and the like.

[0007] On one hand, various methods are proposed to improve feeling, touch to the skin, flexibility and like as nonwoven fabrics used to the absorbent article. First of all, melt blown nonwoven fabric which has fiber diameter of several μm has point of advantage that feeling is soft. However, on the other hand, it is actual circumstances that the melt blown nonwoven fabric is almost not used to the absorbent by itself, since problem of characteristic such as that the nonwoven fabric is low in strength, very low in bending rigidity, fuzzing is occur, threads are easily drawn, incidental looping is easily occurred at the spinning time, rough feeling exist and this stimulate the skin and the like, or productivity is low, thus cost become higher.

[0008] On account of this, various laminated nonwoven fabric which are composite feeling of the melt blown nonwoven fabric and respective characteristic such as strength, bending rigidity, productivity and the like of the spunbonded nonwoven fabric are proposed. For example, (2) Japanese Patent Laid Open No. 88056/1990 proposed laminated nonwoven fabrics which specified laminating condition, and (3) Japanese Patent Laid Open No. 143853/1997 proposed a laminated nonwoven fabrics which comprises a composite spunbonded nonwoven fabric composed of two kind of resins having difference of melting points of 10° C. or more and superposed thereon two kind of melt-blown nonwoven fabric having difference of melting points of 10° C. or more, and fused a resin with a nonwoven fabric having low melting point. However, the feeling in this case is carried by the melt-blown nonwoven fabric, the above described problem which is characteristic of the surface of the melt-blown nonwoven fabric is not still dissolved. And also, the composite nonwoven fabric makes complex the manufacturing apparatus, and melting points between the composite resins and fluidity are different, thus spinning is difficult in some case.

[0009] On account of this, methods to improve feeling and the like of the spunbonded nonwoven polypropylene fabric having excellent strength and productivity are requested. As the improving method of feeling of the spunbonded nonwoven fabric, first of all to make fine the fiber diameter is considered. However, when the fiber diameter is make too fine, strength is lowered, and also bending rigidity, that is, sturdiness of the nonwoven fabric is decreased, in the manufacturing of the absorbent article such as disposable diaper and the like by post processing, in process of sending out of the nonwoven fabric, sealing and the like, it becomes problem that automation and high speed manufacturing becomes difficult, and large amount and low cost product is not obtained, therefore putting the nonwoven fabric to practical becomes difficult in some case.

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[0010] On account of this, there is a method using copolymers of propylene with the other olefin. However, also in this case, though feeling is improved considerably, this is due to lowering of bending rigidity (softening of the raw material resin, that is lowering of elastic modulus), lowering of post processability is not changed. And also, spinability is lowered.

[0011] Further, (4) Japanese Patent Laid Open No. 88459/1998 proposed a long fiber nonwoven fabric composed of a heat fusible conjugate long fiber which comprises at least one kind of low melting point or low softening point resin selected from olefinic copolymer and olefinic terpolymer as the first component, and a crystalline thermoplastic resin as the second component, in which a hydrocarbon based lubricant is contained in at least the first component, and content of the above described hydrocarbon based lubricant is 2 to 20 mass % as the concentration in the fiber.

[0012] That is, this proposal intend to improve lowering of spinability caused by using a low melting point of soft propylene random copolymer as polypropylene resins for improvement of flexibility or touch to the skin of the nonwoven fabric, by adding of the hydrocarbon based lubricant. Consequently, characteristics such as heat resistance, strength, bending rigidity and the like, which are essentially afforded to polypropylene resins, especial polypropylene homopolymer, are lost and also the copolymer further contains relatively large amount of the hydrocarbon based lubricant having low molecular weight and low melting point, for example, lowering of heat sealing property, adhesive property and the like of the nonwoven fabric by bleeding of these lubricants is afraid.

[0013] Moreover, it is known that a conjugate nonwoven fabric made by conjugate spinning with core sheath structure or side-by-side structure of two kind of resins having different kind and melting point, as described in the above described Japanese Patent Laid Open No. 88459/1998 as the nonwoven fabric. However, although this conjugate fiber nonwoven fabric is improved heat fusibility, in the case of increasing proportion of a comonomer in the low melting point of polypropylene resin, there is slimy feeling of the surface as the nonwoven fabric, dry feeling as the surface material of absorbent article such as disposable diaper, napkin or the like is lowered, and give discomfort feeling in some case.

[0014] (5) Japanese Patent Laid Open No. 290381/1999 disclosed a back sheet for the absorptive article which comprises a laminate layered alternately layers composed of polypropylene melt-blown nonwoven fabric and layers composed of polypropylene wet process nonwoven fabric in which one side surface layer of the laminate comprises the polypropylene wet process nonwoven fabric layer. That is, by adopting a short fiber wet process nonwoven fabric, it is intended to secure slipping property of the surface and liquid barrier property. However, the diameter of the fiber of the wet process nonwoven fabric is relatively finer, bending rigidity is lowered, there is a problem of causing complex in the manufacturing method and also lowering the post processability.

[0015] Further, (6) Japanese Patent Laid Open No. 293554/1999 disclosed a heat fused nonwoven fabric which comprises conjugate short fibers having fiber diameter of 10 to 15 μm on at least surface layer, in which a coefficient of

friction (MTU) of the nonwoven fabric is 0.25 or less, and reflectance per unit area is 1.2% or more. However, only a nonwoven fabric composed of conjugate short fibers having a fiber diameter of 13 μm and a fiber length of 45 mm, which having a core sheath structure of high density polyethylene as the sheath component and polyester as the core component is disclosed concretely in examples.

[0016] Furthermore, as improvement of feeling in a spunbonded nonwoven fabric, (7) Japanese Patent Laid Open No. 92856/1996 disclosed a manufacturing method of a nonwoven fabric having excellent flexibility and touch to the skin, in which a propylene ethylene block copolymer having ethylene content of 0.5 to 8 mass % was used, filament groups having knot on the surface were obtained, thereafter corona treated and thermocompression bonded with heating rolls. However, this method has problem in the production cost and the like, and also has great restriction, which cannot apply to most general polypropylene homopolymer.

[0017] Still more, (8) Japanese Patent Laid Open No. 160463/2000 disclosed a flexible nonwoven fabric containing filers composed of polyolefin thermoplastic resin containing olefinic elastomer. And also at the same time, a fabric and a multi layer nonwoven fabric composed of a side-by-side type fiber used the above-described resin and a core sheath type conjugate fiber used the above described resin as core is disclosed. However, the polyolefin thermoplastic resin composing of the fiber of the nonwoven fabric is an object by commonplace way of thinking so as to improve flexibility of the nonwoven fabric, by combining the olefinic elastomer as the soft component, as the result the fiber itself become flexible, sturdiness as the nonwoven fabric is greatly decreased, and post processability is lowered.

[0018] As described above, the conventional improving technique of flexibility, feeling, touch to the skin and the like of the spunbonded nonwoven polyolefin resin fabric is not held characteristic of the spunbonded nonwoven polypropylene fabric itself. That is, the technique abandon characteristic of the spunbonded nonwoven fabric which it can be manufactured with good productivity and low cost, and has excellent strength, bending rigidity and post processability, it is owing to only making the fiber diameter into fine, adopting of the soft resin, making short fiber, conjugate spinning, or laminating of these with the spunbonded nonwoven fabric and the like.

[0019] Consequently, especially, from post processability such as spinability, bending rigidity or the like, as to the nonwoven fabric, it is actual circumstance that the spunbonded nonwoven polypropylene fabric is used still in spite of poor feeling, touch to the skin or the like.

[0020] On account of this, it is strongly expected improvement of the problem such as flexibility, feeling, touch to the skin and the like, while maintaining strength, gas permeability, especially bending rigidity of the polypropylene spunbonded nonwoven fabric from producer and user of the absorbent article such as disposable diaper.

[0021] An object of the present invention is to provide a nonwoven polyolefin fabric and an absorbent article which capable of using suitably for the absorbent article especially such as the disposable diaper, the sanitary napkin and the like, while holding substantially characteristic such as heat resistance, strength, bending rigidity, or the like, which the

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spunbonded nonwoven polypropylene resin fabric has substantially, and also having excellent flexibility, feeling, touch to the skin or the like.

DISCLOSURE OF THE INVENTION

[0022] The present inventors investigate wholeheartedly as to the polyolefin resin, especially the spunbonded nonwoven polypropylene fabric while making the most of function such as gas permeability, flexibility, strength, bending rigidity, heat resistance, post processability, automation suitability and the like afforded to the spunbonded nonwoven polypropylene resin fabric, and also feeling of use, which requested to the end product of the nonwoven fabric, especially the absorbent article, such as spinability, feeling, touch to the skin and the like of the obtained nonwoven fabric. As the result, it is found that feeling of use such as flexibility, feeling, touch to the skin and the like can greatly improved, even though in the spunbonded nonwoven fabric composed of the same fiber diameter, the same METSUKÉ and the same resin, by controlling its friction characteristic, and the present invention is completed based on this knowledge.

[0023] That is, the present invention provides

[0024] (1) A spunbonded nonwoven fabric which comprises a spunbonded nonwoven fabric composed of a polyolefin resin and has an average fiber diameter of 5 to 60 μm , METSUKÉ of 5 to 200 g/m^2 and a coefficient of static friction of 0.1 to 0.4.

[0025] (2) The spunbonded nonwoven fabric according to the above described (1), wherein the nonwoven fabric contains a lubricant.

[0026] (3) The spunbonded nonwoven fabric according to the above described (1) or (2), wherein the lubricant is a fatty acid amide compound, and its content is 0.05 to 1.0 mass %.

[0027] (4) The spunbonded nonwoven fabric according to any one of the above described (1) to (3), wherein the polyolefin resin is polypropylene resin.

[0028] (5) The spunbonded nonwoven fabric according to any one of the above described (1) to (4), wherein the fiber is hydrophilicity imparting treated.

[0029] And also, the present invention provides

[0030] (6) A spunbonded nonwoven fabric which comprises a spunbonded nonwoven polypropylene resin fabric having stiffness (bending resistance), which is the sum of the values for the longitudinal and transverse directions as obtained according to JIS L1096 6.19.1, method A that is 45° cantilever method, of 70 to 120 mm, and a coefficient of static friction of 0.1 to 0.4.

[0031] (7) The spunbonded nonwoven fabric according to the above described (1), wherein the nonwoven fabric has the average fiber diameter of 10 to 30 μm , and METSUKÉ of 10 to 30 g/m^2 .

[0032] (8) The spunbonded nonwoven fabric according to the above described (7) or (8), wherein the nonwoven fabric contains the lubricant of 0.15 to 1.0 mass %.

[0033] (9) The spunbonded nonwoven fabric according to the above described (8), wherein the lubricant is a fatty acid amide compound.

[0034] (10) The spunbonded nonwoven fabric according to any one of the above described (6) to (9), wherein the fiber constituting of the nonwoven fabric is hydrophilicity imparting treated.

[0035] Further, the present invention provides

[0036] (11) An absorbent article made by using the nonwoven fabric according to any one of the above described (1) to (10).

[0037] (12) The absorbent article according to the above described (11), wherein the absorbent article is a disposable diaper, a sanitary napkin or incontinence pad.

BRIEF DESCRIPTION OF DRAWING

[0038] FIGURE 1 is an illustration view of relation of degree of bending rigidity and coefficient of static friction of the spunbonded nonwoven fabric in examples of the present invention and comparative example.

BEST MODE TO CARRYING THE INVENTION

[0039] In the following description, the present invention will be described in further detail.

[0040] [The First Embodiment]

[0041] The nonwoven polyolefin resin fabric of the present invention comprises the spunbonded nonwoven fabric having the average fiber diameter of 5 to 60 μm , METSUKÉ of 5 to 200 g/m^2 , and the coefficient of static friction of 0.1 to 0.4. The nonwoven fabric of the present invention may be any object satisfying the range of the coefficient of static friction of 0.1 to 0.4 as the nonwoven fabric, its means to control the coefficient of static friction may be optional, and is considered adoption of various means. However, the reason why the spunbonded nonwoven fabric of the present invention has excellent flexibility and feeling is considered an effect by improvement of slipping property among long fibers, so that it is preferred a material which improves slipping property of not only fibers on the surface part of the nonwoven fabric, but also fibers as whole the nonwoven fabric, as the result, and a coefficient of static friction as the surface characteristic become in a specific range.

[0042] (Basic Characteristic of Nonwoven Fabric)

[0043] The fiber diameter of the fiber composing the spunbonded nonwoven fabric is 5 to 60 μm , preferably 5 to 40 μm , and 15 to 30 μm for especially the absorptive article such as the disposable diaper or the like. Here, in the case of 5 μm or less, strength and bending rigidity are insufficient, and also in the some case post processability is lowered, and at the same time the using field is greatly limited. Moreover, in the case of 60 μm or more, flexibility is lowered, characteristics as the nonwoven fabric is lost, and also in the some case especially application to the absorptive article, various clothes becomes difficult.

[0044] Moreover, METSUKÉ of the spunbonded nonwoven fabric of the present invention is in the range of 5 to 200 g/m^2 , preferably 7 to 60 g/m^2 , especially 10 to 30 g/m^2 for the absorbent article such as the disposable diaper or the like. Here, in the case of METSUKÉ of 5 g/m^2 or less, in some case strength is insufficient, bending rigidity (sturdiness) is lower, and post processability is fallen. Moreover, in

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the case of 200 g/m² or more, flexibility, gas permeability or the like is lowered, thus characteristics as the nonwoven fabric are lost, and in some case usage becomes difficult due to use.

[0045] The spunbonded nonwoven fabric can select/combine properly the resin, the fiber diameter, METSUKO and the like, based on the use of the nonwoven fabric, required property, gas permeability, non-water permeability or the like.

[0046] The spunbonded nonwoven polyolefin resin fabric of the present invention is not especially restricted as far as it is the spunbonded nonwoven fabric, and it can produce by various manufacturing process. Moreover, the bonding form can adopt embossing, calendaring, heat adhesion such as hot air or the like, mechanical entangling such as needle punching, water punching and the like. However, heat adhesion by embossing is preferred from productivity.

[0047] (Coefficient of Static Friction)

[0048] The characteristic of the present invention is that the nonwoven fabric of the spunbonded nonwoven fabric comprising conventional well known polyolefin resin has the coefficient of static friction of 0.1 to 0.4, preferably 0.12 to 0.35. Here, in the case of the coefficient of static friction is 0.1 or less, processability is lowered by over slippage in the post processability, and at the same time the usage amount of additives or surface treatment agent adopted general is necessary due to lowering of the coefficient of static friction, in some case economic performance is fallen. Further, in some case thermal sealing at the time of post processing, conjugation property by adhesives and the like is trended toward poor, thus such case is not preferred. Moreover, in the case of 0.4 or more, improving effect of feel of usage such as flexibility, feeling, touch to the skin become insufficient.

[0049] (Measurement of Coefficient of Static Friction)

[0050] The coefficient of the spunbonded nonwoven fabric of the present invention can determine according to ASTM-D 1894. Concretely, based on measuring conditions of:

[0051] Measuring machine of a coefficient of static friction: made of Toyo Seiki Seisakusho Co. Ltd., AN type

[0052] Loading plate: 63.6 mmx102.2 mmx19.4 mm (height)

[0053] Load: 8.87N of iron plate

[0054] Incline speed: 2.7 degree/second

[0055] sliding angle θ was determined by piling up measuring surfaces of the nonwoven fabric, $\tan \theta$ was obtained, and made it the coefficient of static friction. The smaller the numerical value the better the slipping property.

[0056] (Polypropylene Resin)

[0057] The polyolefin resin used in the spunbonded nonwoven polyolefin resin fabric of the present invention is not especially restricted, it can include a homopolymer of propylene, copolymer of propylene with at least one of α -olefin such as ethylene, butene-1, 4-methyl-pentene-1, hexane-1, octen-1 or the like. These polypropylene resins are selected properly from those that having difference of various crystallinity, molecular weight and distribution of molecular

weight from selection of catalysts at the time of polymerization, polymerization condition or the like, based on the property required in the nonwoven fabric. This selection is examined from the points of strength, bending rigidity, use and the like, but from spinability, vending rigidity, slimy feeling or the like as described above, using of the homopolymer of propylene or the polypropylene copolymer with low ratio of copolymerization is preferred.

[0058] Here, crystallinity is selected from a range from 88 to 95 mol %, preferably 89 to 93 mol % in the isotactic pentad fraction in the case of using the nonwoven fabric as the disposable diaper and the like. Here, the isotactic pentad fraction (IPF) is an isotactic fraction in the pentad unit in the polypropylene molecular chain, which is measured by using nuclear magnetic resonance spectrum (¹³C-NMR) by an isotope carbon for example described in Macromolecules, vol. 28, No16, pp5403 (1995).

[0059] Moreover, melt flow rate (MFR) [according to JIS K 7210, measuring temperature: 230° C., measuring load: 21.18N] of the polypropylene resin is in the range of 5 to 200 g/10 min, preferably 10 to 100 g/10 min. In particular, those that in the range of 30 to 80 g/10 min is suitable for the absorptive material.

[0060] (Polyethylene Resin)

[0061] Next, polyethylene resins include a homopolymer of ethylene, copolymers of ethylene with α -olefin having 3 to 10 carbon atoms such as propylene, butene-1, 4-methyl-pentene-1, hexane-1, octane-1 or the like, and copolymers of ethylene with a polymerizable monomer such as vinyl acetate, acrylic acid or the like. In particular, the above described ethylene- α -olefin copolymer having density of 880 to 960 kg/m³, preferably 900 to 950 kg/m³, melting point in the range of 100 to 140° C., preferably 110 to 130° C., and melt flow rate (MFR) [according to JIS K 7210, measuring temperature: 190° C., measuring load: 21.18N] of 5 to 60 g/10 min, preferably 10 to 50 g/10 min is used preferably from points of spinability, melting point, bending rigidity.

[0062] Moreover, these polypropylene resins and polyethylene resins may be mixtures of two kind or more respectively, and can use as resin compositions containing other ethylene resin, propylene resin, thermoplastic elastomer or the like of less than 50 mass %.

[0063] (Controlling Method of Coefficient of Static Friction)

[0064] Next, means to obtain the spunbonded nonwoven fabric having the coefficient of static friction in the range of 0.1 to 0.4 are not restricted especially, and various means are included. Concretely, it can exemplify roughly divided to (1) melt spinning process by combining a lubricant into a polyolefin resin for spinning, and (2) surface treating process to the fiber after spinning.

[0065] (Lubricant)

[0066] Here, the lubricant is not especially restricted, and include fatty acid amide compound, fatty acid compound, paraffin and hydrocarbon resin, silicone compound, silicone polymer, fluorine compound, fluorine polymer such as copolymer of tetrafluoroethylene with propylene, copolymer of vinylidene fluoride with hexafluoroethylene or the like, or these mixture. Among them the fatty acid amide compound is preferably used.

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[0067] The fatty acid amide compound include fatty acid monoamide compound, fatty acid diamide compound, saturated fatty acid monoamide compound, unsaturated fatty acid diamide compound. Concretely, it includes amide laurate, amide myristate, amide palmitate, amide stearate, amide behenate, amide oleate, amide erucate, amide montanate, amide N,N'-methylene-bis-laurate, amide N,N'-methylene-bis-myristate, amide N,N'-methylene-bis-palmitate, amide N,N'-methylene-bis-behenate, amide N,N'-methylene-bis-oleate, amide N,N'-methylene-bis-erucate, amide N,N'-ethylene-bis-oleate, amide N,N'-ethylene-bis-erucate and the like, and also these can be used by combining plural kind of substances.

[0068] Among these fatty acid amide compounds, amide erucate, which is an unsaturated fatty acid monoamide compound, is preferably used. The reason why it is used is they are suitable to decrease the coefficient of static friction of the nonwoven fabric, by decreasing of spinability by exposing unnecessarily the fatty acid amide on the surface at the time of spinning of the fiber of the nonwoven fabric, and ageing of the nonwoven fabric containing the fatty acid amide compound described below. Content of the fatty acid amide compound in the polyolefin resin is in the range of 0.05 to 1 mass %, preferably 0.1 to 0.5 mass %. This content is decided by judging synthetically kind of the polyolefin resin, the resin characteristics such as crystallinity, MFR and the like, kind of the fatty acid amide compound, required property of the obtained nonwoven fabric, ageing condition and the like.

[0069] Consequently, for example, in the case of using amide erucate in the homopolymer of propylene having isotactic pentad fraction of around 90 mol %, it is preferred in the range of 0.1 to 0.5 mass %, especially 0.2 to 0.4 mass %. In this case, although it depends on ageing treatment condition, if it is 0.2 mass % or less, in some cases it is difficult to control the coefficient of static friction of the nonwoven fabric in the range of 0.1 to 0.4, and if it is 0.4 mass % or more, in some cases the amount of the amide erucate on the surface of the nonwoven fabric is much, it becomes cause of worse of appearance such as generation of white powder or the like, or lowering of heat fusion property and post processability.

[0070] Further, the spunbonded nonwoven polyolefin resin fabric of the present invention can be added well-known additives component used generally in the nonwoven fabric for use or imparting characteristic or the like. These well known additives components include neutralizing agents such as calcium stearate, hydrotalcite or the like, antioxidants such as phenol based, phosphorus based, sulfur based or the like, heat stabilizers, nucleus forming agents, UV absorbers, light stabilizers, antistatic agents, flame retardants, pigments, dyes, or inorganic powders such as silica, talc, calcium carbonate, calcium oxide, magnesium oxide or the like.

[0071] (Melt Spinning)

[0072] The spunbonded nonwoven polyolefin resin fabric of the present invention make a spunbonded primary nonwoven fabric by melt spinning a mixture which is dry bled fixed amount of lubricant such as fatty acid amide or the like and additives component added as the need arises to a polyolefin resin.

[0073] Here, the spunbonded nonwoven fabric can be obtained, for example, a primary nonwoven fabric by well

known method which comprises melt extruding the raw material polyolefin resin having the above described combination, spinning it from a spinneret for spinning, taking up the spun fiber with an airborne tracking apparatus such as air sucker or the like, opening as the need arises, collecting fibers with air flow by a web collecting apparatus such as a net conveyer or the like, partial fusing with heating means such as heated air, heating roll or the like, thereafter winding up.

[0074] Further, this spunbonded nonwoven polyolefin resin fabric is a nonwoven fabric comprising ordinarily polyolefin resin alone, but it may be a conjugate fiber nonwoven fabric comprising a polyolefin resin of at least 50% on the surface of the fiber.

[0075] These composite fiber nonwoven fabric may be used the composite fiber having core-sheath structure composing of a polyolefin resin as the sheath component and a resin having higher melting point than the sheath component resin excepting the polyolefin resin such as a polyamide resin, polyester resin or the like as the core component, or the conjugate fiber having side-by-side structure which comprises the polyolefin resin of ordinarily 50 mass % or more of fibers and the other resin in the rest. Further, this core-sheath structure conjugate fiber and side-by-side structure conjugate fiber may be, of course, combination of two kind of different polyolefin resins among polyolefin resins.

[0076] (Ageing Processing)

[0077] Thus obtained spunbonded primary nonwoven fabric is excellent in spinability, however in some cases the coefficient of static friction specified by the nonwoven fabric of the present invention is not expressed by itself, by the kind of the lubricant, especially in the case of the fatty acid amide compound. In this case, to make the spunbonded nonwoven polyolefin resin fabric of the present invention, by only after ageing this primary nonwoven fabric under heating, it can be the range of the coefficient of static friction which is specified by the present invention. In the conventional nonwoven fabric manufacturing apparatus, such ageing apparatus is not included, generally ageing was not performed.

[0078] Here, ageing condition is differed due to kind of the polyolefin resin, resin characteristic such as degree of crystallinity, density, melting point or the like, kind and melting point of contained the fatty acid amide compound and solubility to the polyolefin resin or the like. Consequently, by considering characteristic of the polyolefin resin which is the raw material of the nonwoven fabric, or characteristic of the fatty acid amide compound as the lubricant, and by considering the range of the coefficient of static friction in the range of 0.1 to 0.4, required characteristic such as flexibility, feeling, touch to the skin or the like required to the end product, concretely the treating condition is decided experimentally.

[0079] For example, the spunbonded nonwoven polyolefin resin fabric of the present invention is obtained by ageing a spunbonded nonwoven fabric made by melt spinning the polyolefin resin which containing the fatty acid amide compound at a temperature of 30 to 60° C. for around 1 to 50 hours. For example, in the homopolymer of polypropylene, as a concrete example in the case of that having isotactic pentad fraction of around 90 mol % and content of amide erucate of 0.3 mass %, the following ageing treatment condition can set up.

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[0080] In the case of the ageing temperature of 40° C., the ageing time is 5 to 50 hours, preferably about 8 to 12 hours. Moreover, in the case of the ageing time is 24 hours, the ageing temperature is 32 to 50° C., preferably about 33 to 40° C. When the ageing condition is milder than the range described above, lowering of the coefficient of static friction requires longer time, in some cases productivity is lowered. Further, when the ageing condition is severer than the above described range, in some cases the coefficient of static friction become higher reversely, thus it is not preferred.

[0081] This ageing treatment can ordinarily carried out in an ageing room which heated air is circulated, by arranging core pipes in the state of winding the nonwoven fabric in roll form. When this ageing is performed, even though the nonwoven fabric is wound state in roll form, the nonwoven fabric is obtained approximate uniform effect of ageing treatment due to gas permeability of the nonwoven fabric. Further, ageing can also carried out by roll heating and/or heated air, the nonwoven fabric is not wound state, but while it is running between rolls.

[0082] (Surface Treatment)

[0083] Next, the other method to give the coefficient of static friction of the nonwoven fabric of the present invention is a method by surface treatment of the fiber of the nonwoven fabric obtained by spinning. As the surface treating agent, for example, a polution of dimethyl siloxane, methyl hydrogen polysiloxane, compound containing fatty acid amide can be used. However, this surface treatment has problem that cannot treat into inner part in some cases, due to wet eating process, drying process and thickness of the nonwoven fabric. Therefore, in many cases the methods by melt blending of the lubricant described above is preferred, due to form, use, range of the coefficient of static friction or the like of the nonwoven fabric.

[0084] The spunbonded nonwoven fabric comprising the polyolefin resin of the present is generally hydrophobically, owing to use of the absorptive articles and the like, for example, in the case of using as the top material of the disposable diaper or sanitary napkin or the like, in some cases hydrophobicity of at least water or the like permeable is required. In this case the nonwoven fabric can do hydrophobicity imparting treatment.

[0085] This hydrophobicity imparting treatment include introduction of hydrophilic groups such as carboxyl group or the like by ozone treatment, or surface treatment by hydrophilic compounds, however treatment by solution of hydrophilic compounds is preferred in the point of the effect. As the treating method, spraying method, coating method, immersing method and the like can be exemplified. Moreover, the hydrophilic compound can be exemplified, for example, alkyl-ester such as polyalcohol having 8 to 26 carbon atoms containing polyoxyethylene, alkyl-ether, polyether containing fatty acid amide group, fatty acid monoglyceride, sorbitol ester derivative, alkyl phosphate metal salt, polyoxyethylene alkyl ether sulfate metal salt, alkyl sulfosuccinate metal salt, sugar derivative having glucose ring and the like.

[0086] The spunbonded nonwoven fabric composed of the polyolefin resin of the present invention is maintained essential characteristic of the nonwoven fabric which has the polyolefin resin itself, by lowering of the coefficient of static

friction by the ageing treatment or the surface treatment, and flexibility, feeling, touching feel such as touch to the skin, and usage feel are improved markedly. Consequently, it can be used as materials for various absorbent article (such as sanitary material and the like), various clothing materials, material for medical treatment, material for wrapping and the like.

[0087] (Forming of Multilayer)

[0088] The spunbonded nonwoven fabric can make a multilayer material with other nonwoven fabric, thermoplastic resin film, paper or the like. However, in the case of used as multilayer object, at least one side of the nonwoven fabric is used the nonwoven fabric of the present invention which satisfy the above described characteristics such as the coefficient of static friction of 0.1 to 0.4. And, the other nonwoven fabric in the case of using the spunbonded nonwoven polyolefin resin fabric in the multilayer nonwoven fabric may be a nonwoven fabric which composed of not the polyolefin resin but the polyamide resin or the polyester resin.

[0089] The characteristic related to feel of the nonwoven fabric is the problem on the surface of the nonwoven fabric material, to improve the characteristics such as strength, moisture permeability, gas permeability, powder barrier property, heat fusibility and the like, it can also be made the multilayer material with general polyolefin resin nonwoven fabric containing no the fatty acid amide compound, other thermoplastic resin nonwoven fabric, the moisture permeable film, water resistant film, water-proofing film or the like.

[0090] In this case, usually the spunbonded nonwoven polyolefin resin fabric after the above described ageing treatment is laminated so as to exposure on at least one side. However, owing to the case, it can also be ageing treated after lamination with other nonwoven fabric or film or the like. The other nonwoven fabric in this case include the melt-blown nonwoven fabric, short fiber nonwoven fabric or the like. For example, a laminating method where the melt-blown nonwoven fabric is spun on the spunbonded nonwoven fabric, and further spunbonded nonwoven fabric is manufactured in multi-step and continuously thereon, a multi-layer nonwoven fabric is previously manufactured by containing fatty acid amide into a polyolefin resin for at least one side of spunbonded nonwoven fabric, and then this multi-layer nonwoven fabric is ageing treated is given.

[0091] Here, the nonwoven fabric except the polyolefin resin can include a nonwoven fabric, for example, of the polyester resin, the polyamide resin, especially having melting point of 150° C. or more, particularly 150 to 300° C. Here, the polyester resin can include homopolyester such as polyethylene terephthalate, polybutylene terephthalate, polytrimethylene terephthalate, polynaphthalene terephthalate and the like, and copolyester which copolymerized with other component, in which the homopolyester is main component unit, and further these blended polyester.

[0092] The polyamide resin can exemplify nylon 6 (polycaprolactamide), nylon 6,6 (polyhexamethylene adipamide), nylon 6,10 (polyhexamethylene sebacamide), nylon 11 (polyundecane amide), nylon 7 (poly- ω -aminohexanoic acid), nylon 9 (poly- ω -aminononanoic acid), nylon 12 (poly-lauric amide) and the like. Among them, nylon 6 and nylon 6,6 are used preferably.

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[0093] As the laminating means to form his multilayer nonwoven fabric, various laminating means such as heat adhesion, adhesion with adhesives and the like is given. However, simple and low cost laminate heat adhesion means, especially heat embossing roll method can be adopted. This embossing roll method can laminate by using well-known laminating apparatus with an embossing roll and a flat roll. Here, the embossing roll can adopt various shape embossing pattern, there are lattice state in which each fused part is continued, independent lattice state, optional distribution and the like. Moreover, emboss area fraction is in the range of approximate 5 to 40%.

[0094] Further, the spunbonded nonwoven polyolefin resin fabric can also make the multilayer material with moisture permeable resin layer (film), the water resistant resin layer (film), and the water-proofing resin layer (film) in addition to lamination with the other nonwoven fabric. In this case, an extruding laminating method, a heat embossing roll method, a dry laminating method and the like can adopt.

[0095] The heat embossing roll lamination condition is different by melting point of the spunbonded nonwoven fabric or the other nonwoven fabric, and making either layer of other film the emboss side, the condition is selected properly by taking respective factor into consideration. These emboss pattern, emboss area fraction, temperature, pressure and the like can be properly selected depending on the fiber diameter, thickness, METSUKU, gas permeability, processing speed of each nonwoven fabric, and further melting point, thickness and the like of other nonwoven fabric film or the like.

[0096] The spunbonded nonwoven fabric is used for, including the disposable diaper, sanitary napkin or incontinence pad, medical treatment, clothing and wrapping.

[0097] [Examples Based on the First Embodiment]

[0098] In the following, the present invention will be illustrated in further detail based on the manufacturing examples of the spunbonded nonwoven fabric based on the first embodiment. However, the present invention is not limited by these examples.

EXAMPLE 1

[0099] To a crystalline polypropylene resin [isotactic pentad fraction: 91 mol %, MFR: 60 g/10 min, melting point: 160° C.] 100 mass parts, a phenol based antioxidant (made of Ciba Special Chemical Company, Irganox 1010): 0.035 mass parts, phosphorus based antioxidant (made of Sando Company, Sandostab P-EPQ): 0.035 mass parts, a neutralizer (made of Kyodo Yakuhin Co. Ltd., calcium stearate) 0.025 mass parts and amide erucate: 0.3 mass parts were dry blended with a super-mixer, thereafter melt kneading at 220° C. by using 65 mm ϕ extruder, and melt spun by extruding from the spinneret. The spinneret in this case was diameter of hole of the spinneret: 0.3 mm, and numbers of it in width direction: 200, and extrusion direction: 15.

[0100] Then, the spun fiber group were introduced into an air sucker and tracked and drawn, and collected on a belt having a suction apparatus, and then it was sent to heated embossing rolls [an embossing roll at 140° C./a flat roll at 140° C.] and partly adhered, and then rolled it onto a paper tube, thus a primary nonwoven fabric was obtained. The obtained rolled nonwoven fabric was ageing treated in an

ageing condition of 40° C./24 hours to obtain a spunbonded nonwoven polyolefin resin fabric of the present invention. The obtained nonwoven fabric had an average fiber diameter: 16 μ m, METSUKU: 20 g/m², a coefficient of static friction: 0.19, degree of bending rigidity: 5.3 cm, touch to the skin: \odot , feeling: \odot , and end breakage or jogging in the spinning process was not observed, and it can spun stably.

[0101] Further, evaluation of the nonwoven fabric was performed based on the following description.

[0102] (1) Coefficient of Static Friction

[0103] Measurement was performed according to the measuring method of the coefficient of static friction of ASTM-D 1894. And, the detail was described above.

[0104] (2) Degree of Bending Rigidity [Longitudinal Direction] (cm)

[0105] Measurement was performed according to JIS L 1096 (45° cantilever method).

[0106] (3) Touch to the skin-feeling

[0107] A functional test by touch to the skin-handle by 20 monitors was performed, and evaluation of \odot , \circ and Δ was performed.

EXAMPLE 2

[0108] An experiment was performed according to example 1 except that changing the content of amide erucate to 0.4 mass parts, the aperture of spinneret to 0.3 mm, extruding speed and belt speed. The obtained nonwoven fabric had an average fiber diameter: 24 μ m, METSUKU: 20 g/m², a coefficient of static friction: 0.19, of stiffness: 5.3 cm, touch to the skin: \odot , feeling: \odot . And end breakage or jogging in the spinning process was not observed, and it can spun stably.

[0109] [The Second Embodiment]

[0110] A spunbonded nonwoven polypropylene resin fabric of the present invention is a spunbonded nonwoven fabric which has stiffness [sum of the value for the longitudinal and transverse directions as obtained according to JIS L 1096, 6.19.1, method A (45° cantilever method)] of 70 to 120 mm and a coefficient of static friction of 0.1 to 0.4.

[0111] (Stiffness)

[0112] That is, spunbonded nonwoven fabric has, first of all, has stiffness [sum of the values for the longitudinal and transverse directions as obtained according to JIS L 1096, 6.19.1, method A (45° cantilever method)] of 70 to 120 mm. As the item of evaluation of performance of the spunbonded nonwoven fabric is considered feeling together with strength and the like as important. This feeling is considered as combination of softness, hardness, resiliency, restitution property, feeling of cold temperature, luster, draping property and the like, and it is well known that feeling is different greatly by the manufacturing method, especially adhesion method.

[0113] Among these properties, degree of bending rigidity by the evaluation test of flexibility, which is index of softness, is standardized various test method depending to characteristic of the nonwoven fabric. The spunbonded nonwoven fabric of the present invention is specified by the measuring value by the above described 45° cantilever

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method, which is suited to evaluation of flexibility of the most general nonwoven fabric. The stiffness of the spunbonded nonwoven fabric is usually observed difference of stiffness, in flow direction (longitudinal) and direction at right to flow (transverse) in the manufacturing process of the nonwoven fabric. Consequently, in the spunbonded nonwoven fabric of the present invention, to make the average this property of direction, stiffness was specified with sum of stiffness in longitudinal-transverse direction. (In the following, sum of values of stiffness for the longitudinal and transverse direction is used as the stiffness as far as especially not making any comment.

[0114] The stiffness of the spunbonded nonwoven polypropylene resin fabric, which is general purpose article having the fiber diameter of approximate 20 μm and METSUKU of 20 g/m^2 , is approximate 70 to 120 mm. It is said that the stiffness is desirable low for feeling. As means to lower stiffness, it has been investigated means which to finer the fiber diameter, to decrease METSUKU, to adopt low crystalline resin as the polypropylene resin, and further to lower elastic modulus of the polypropylene resin by combining soft resin or thermoplastic elastomer to the polypropylene resin and the like.

[0115] However, the spunbonded nonwoven polypropylene resin fabric require not only feeling but also balance of synthetic properties. The method to improve feeling by lowering the degree of stiffness described above is that to soften the polypropylene resin itself, or to decrease fiber diameter or METSUKU. This can to say improving means that sacrifice strength and moderate flexibility, which are fundamental special character of the spunbonded nonwoven polypropylene resin fabric.

[0116] Consequently, at manufacturing time of the spunbonded nonwoven fabric or, especially, in processing into the end product such as disposable diaper, stabilization of the nonwoven fabric at the post processing time such as sending out of the nonwoven fabric, heat sealing and the like is not maintained, from point of stabilization of quality, productivity and the like, there is limit in technique to only lower the stiffness. Consequently, the spunbonded nonwoven polypropylene resin fabric, which is much consumed, has been used that having stiffness of 70 to 120 mm in spite of existing dissatisfaction in feeling, touch to the skin and the like. And also, for example, even though a spunbonded nonwoven fabric which combined a thermoplastic elastomer of 10 mass % into a polypropylene resin, decreasing of the stiffness is slight, and when combining amount of the thermoplastic elastomer make more much, not only the post processability decrease but also spinability lower.

[0117] (Coefficient of Static Friction)

[0118] Moreover, by investigation of the inventors of the present invention, it was found that the numerical value of the stiffness itself do not showed directly feeling of the spunbonded nonwoven polypropylene resin fabric as described above. That is, it was found that feeling which feel on hand or skin of human can not evaluated by the numerical value of the stiffness alone.

[0119] The spunbonded nonwoven polypropylene resin of the present invention has characteristic which satisfy in addition to the stiffness of 70 to 120 mm, preferably 75 to 115 mm as the first, and the coefficient of static friction in

the range of 0.1 to 0.4, preferably 0.12 to 0.36 as the second. Although the reason why the coefficient of static friction of the spunbonded nonwoven fabric relates greatly to feeling of the nonwoven fabric is not always clear, it is considered that slippage between fibers which constitute the nonwoven fabric become favorable in the case of touching to the hand or skin, and the whole nonwoven fabric become easy deformable. On account of this, evaluation of feeling of the spunbonded nonwoven fabric is difficult by only the stiffness, it became clear that even though the equal stiffness, it was different greatly by the coefficient of static friction.

[0120] The coefficient of static friction of the spunbonded nonwoven polypropylene resin fabric of the present invention may be controlled into 0.1 to 0.4, the means is optional, and is concerned adoption of various means. However, it is considered that the reason why the spunbonded nonwoven fabric of the present invention has excellent flexibility and feeling is the effect by improving of slipping property between the above described long fibers, therefore not only slipping property of the fiber of the surface part of the nonwoven fabric, but also slipping property of the fiber as the whole nonwoven fabric are improved, as the result the coefficient of static friction as the surface characteristic is in the specific range.

[0121] The characteristic of the present invention is that a spunbonded nonwoven fabric is in addition to having specific range of stiffness which secure strength, sturdiness, post processability and the like as conventional well-known spunbonded nonwoven polypropylene resin nonwoven fabric, having the above described coefficient of static friction of 0.1 to 0.4, preferably 0.12 to 0.36. Here, when the coefficient of static friction is 0.1 or less, in addition to lower processability reversely by over-slippage in the post processing, owing to lowering the coefficient of static friction, it require more much usage amount of additives or surface treating agent adopted generally, thus it becomes worse economically in some case. Further, there is trend to lower conjugativity by heat sealing, adhesives and the like at the time of post processing, and it is not preferred in some case. And, when the coefficient of static friction is 0.4 or more, the improving effect of usage feel such as flexibility, feeling, touch to the skin becomes insufficient.

[0122] Moreover, measurement of the coefficient of static friction is as described in paragraph of "measurement of a coefficient of static friction" in the first embodiment described above.

[0123] (Basic Characteristic of Nonwoven Fabric)

[0124] The spunbonded nonwoven polypropylene resin fabric has preferably an average fiber diameter of 10 to 30 μm and METSUKU of 10 to 30 g/m^2 , and more preferably the average fiber diameter of 10 to 25 μm and METSUKU of 15 to 25 g/m^2 . Here, when the average fiber diameter is 10 μm or less and METSUKU is 10 g/m^2 or less, securing the range of strength and stiffness is difficult, as the result post processability become lower. And, when the average fiber diameter is 30 μm or more and METSUKU is 30 g/m^2 , securing of stiffness and feeling is difficult in some case. And flexibility become lower, characteristics as the nonwoven fabric is decreased, especially application to the absorbent article and the like is difficult in some case, and its using field is restricted greatly.

[0125] The spunbonded nonwoven polypropylene resin fabric of the present invention can select/combine properly

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resin, fiber diameter, METSUKÉ and the like based on the use of the nonwoven fabric, required property, gas permeability, non-water permeability and the like.

[0126] The nonwoven polypropylene resin fabric used in the present invention is not especially restricted as far as it is the spunbonded nonwoven fabric, and it can produce by various manufacturing process. Moreover, the bonding form can adopt embossing, calendaring, heat adhesion such as hot air or the like, mechanical entangling such as needle punching, water punching and the like. However, heat adhesion by using heat embossing method is preferred from securing of productivity stiffness and the like.

[0127] This heat embossing roll method is performed by using well-known laminating apparatus having an embossing roll and a flat roll. Here, the embossing roll can adopt various shape embossing pattern, there are lattice state in which each fused part is continued, independent lattice state, optional distribution and the like. And, emboss area fraction is in the range of approximately 5 to 40%. Here, when emboss area fraction is 5% or less, it come off the lower limit of the range of stiffness, and when the emboss area fraction is 40% or more, it come off the upper limit of stiffness, and at the same time flexibility is easily decreased in some case. And, when embossing pressure is low, usage feel such as flexibility, feeling, touch to the skin is favorable, however reversely stiffness is lowered, and post processability is decreased markedly, thus it is not practical. Consequently, condition of heat embossing method is selected properly by taking shape of embossing part, pitch between emboss adhering parts, roll temperature and the like, and stiffness into consideration.

[0128] (Polypropylene Resin)

[0129] In this embodiment, the spunbonded nonwoven fabric used the polypropylene resin described in previously in the first embodiment is suitable. Since the propylene resin is as described previously, redundant explanation is omitted.

[0130] These polypropylene resins may be mixtures of two kind or more, and can use as resin compositions containing other ethylene resin, propylene resin, thermoplastic elastomer or the like of less than 30 mass % according to necessity.

[0131] (Method for Control Coefficient of Static Friction)

[0132] In this embodiment, the coefficient of static friction is controlled by applying the lubricant to the fiber of the nonwoven fabric as same as the first embodiment described above. Since the "lubricant", "melt spinning", "ageing" and "surface treatment" is as described previously in explanation of the first embodiment, redundant explanation is omitted here.

[0133] (Formation of Multilayer)

[0134] Moreover, in this embodiment, the nonwoven fabric may be made the multilayer nonwoven fabric as same as the first embodiment described previously. With regard to formation of multilayer, since it is as described previously in the paragraph of "formation of multilayer", redundant explanation is omitted here.

[0135] [Examples Based on the Second Embodiment]

[0136] In the following, the present invention will be illustrated in further detail based on manufacturing examples

of the spunbonded nonwoven fabric based on the second embodiment. However, the present invention is not limited by these examples.

EXAMPLE 3 to 4, and Comparative Example 1 to 5

[0137] To a crystalline polypropylene resin [isotactic pentad fraction: 91 mol %, MFR: 60 g/10 min, melting point: 160° C.] 100 mass parts, a phenol based antioxidant (made of Ciba Special Chemical Company, Irganox 1010): 0.035 mass parts, phosphorus based antioxidant (made of Sando Company, Sandostab P-EPQ): 0.035 mass parts, a neutralizer (made of Kyodo Yakuin Co. Ltd., calcium stearate) 0.025 mass parts and amide erucate: [mass parts listed in Table 1] were dry blended with a super-mixer, thereafter melt kneading at 220° C. by using 65 mm ϕ extruder, and melt spun by extruding from the spinneret. The spinneret in this case was diameter of orifice of the spinneret in example 1, 2 and comparative example 1 to 4: 0.4 mm, and in comparative example 5: 0.3 mm, and numbers of it in width direction: 200, and extrusion direction: 15.

[0138] Then, the spun fiber group were introduced into an air sucker and tracked and drawn, and collected on a belt having a suction apparatus, and then it was sent to heated embossing rolls [the condition listed in Table 1] and partly adhered, and then rolled it onto a paper tube, thus a primary nonwoven fabric was obtained. By alternating manufacturing condition of the nonwoven fabric, nonwoven fabric having different average fiber diameter, METSUKÉ and degree of adhesion were obtained.

[0139] The obtained rolled nonwoven fabric was ageing treated in an ageing condition of 40° C.: 24 hours to obtain a spunbonded nonwoven polypropylene resin fabric. The average fiber diameter, METSUKÉ, the coefficient of static friction, stiffness, feeling, post processability and result of spinability of the obtained nonwoven fabric are listed in Table 2.

[0140] Further, evaluation of the nonwoven fabric was performed based on the following description.

[0141] (1) Coefficient of Static Friction

[0142] Measurement was performed according to the measuring method of the coefficient of static friction of ASTM-D 1894. And, the detail was described above.

[0143] (2) Stiffness [Sum of the Values for the Longitudinal and Transverse Directions]

[0144] Measurement was performed according to JIS L 1096 6.19.1, method A (45° cantilever method).

[0145] (3) Feeling

[0146] A functional test by touch to the skin-handle by 20 monitors was performed, and evaluation of \odot , \circ and Δ was performed.

[0147] (4) Post Processability

[0148] To the spunbonded nonwoven fabric, by using a nozzle discharge system fiber spray die, an ethylene-vinyl acetate based hotmelt adhesive FI-6805 [made of Nitta Findorei Co. Ltd.,] was sprayed so as to be coating amount of 4 g/m² in fibrous state. And then, it was superposed thereon a drawn PE film containing inorganic filler "Poram

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PU35" (thickness 35 μm) made of Tokuyama and laminated together to obtain a nonwoven fabric laminate. When this lamination, those that got wrinkle-meander-neck-in made Δ , and that laminated without trouble made \odot .

TABLE 1

	umide accurate mass parts	ageing do or don't	embossing condition				spin-ability
			area fraction %	pressure N/cm	temperature ($^{\circ}\text{C}$)	emboss side/flat side	
example 3	0.2	do	20	500	135/135		\odot
example 4	0.2	do	20	500	135/135		\odot
comparative example 1	No	don't	20	500	135/135		\odot
comparative example 2	0.1	do	20	500	135/135		\odot
comparative example 3	No	don't	20	500	135/135		\odot
comparative example 4	0.4	do	10	300	100/10		\odot
comparative example 5	No	don't	20	500	130/130		Δ

[0149]

TABLE 2

	fiber diameter (μm)	METSUKE (g/cm^2)	static friction coefficient	Stiffness (mm)			Post feeling	Process-ability
				Longi-tudinal	Trans-verse	sum		
example 3	18	20	0.18	53	37	90	\odot	\odot
example 4	18	20	0.28	59	38	97	\odot	\odot
comparative example 1	18	20	0.65	64	39	103	Δ	\odot
comparative example 2	18	20	0.45	60	38	98	Δ	\odot
comparative example 3	18	18	0.62	57	38	95	Δ	\odot
comparative example 4	18	20	0.15	39	31	65	\odot	Δ
comparative example 5	14	17	0.55	43	20	63	\odot	Δ

[0150] Further, the relation between the coefficient of static friction and stiffness of spunbonded nonwoven fabric of examples of the present invention and comparative examples is shown in FIGURE 1. It is clear that spunbonded nonwoven fabric of the present invention (in the range of dotted line) is different markedly from conventional nonwoven fabric.

[0151] Industrial Availability

[0152] The present invention is usable as the nonwoven polyolefin resin fabric and the absorbent article used this

nonwoven fabric, and it is especially favorable in flexibility, feeling, touch to the skin, and is excellent in strength, bending rigidity and post processability, and it is usable suitably to various use, especially as the material for the absorbent article such as disposable diaper and the like.

1. A spunbonded nonwoven fabric which comprises a spunbonded nonwoven fabric made of a polyolefin resin and has an average fiber diameter of 5 to 60 μm , METSUKE of 5 to 200 g/m^2 and a coefficient of static friction of 0.1 to 0.4.

2. The spunbonded nonwoven fabric according to claims 1, wherein the nonwoven fabric contains a lubricant.

3. The spunbonded nonwoven fabric according to claims 1 or 2, wherein the lubricant is a fatty acid amide compound, and its content is 0.05 to 1.0 mass %.

4. The spunbonded nonwoven fabric according to any one of claims 1 to 3, wherein the polyolefin resin is a polypropylene resin.

5. The spunbonded nonwoven fabric according to any one of claims 1 to 4, wherein the fiber is hydrophilicity imparting treated.

6. A spunbonded nonwoven fabric which comprises a spunbonded nonwoven polypropylene resin fabric having stiffness, which is the sum of the values for the longitudinal and transverse directions as obtained according to JIS L1096 6.19.1, method A that is 45 $^{\circ}$ cantilever method, of 70 to 120 mm, and a coefficient of static friction of 0.1 to 0.4.

7. The spunbonded nonwoven fabric according to claim 6, wherein the nonwoven fabric has the average fiber diameter of 10 to 30 μm , and METSUKE of 10 to 30 g/m^2 .

8. The spunbonded nonwoven fabric according to claims 6 or 7, wherein the nonwoven fabric contains the lubricant of 0.15 to 1.0 mass %.

9. The spunbonded nonwoven fabric according to claim 8, wherein the lubricant is a fatty acid amide compound.

10. The spunbonded nonwoven fabric according to any one of claims 6 to 9, wherein the fiber constituting of the nonwoven fabric is hydrophilicity imparting treated.

11. An absorbent article made by using the nonwoven fabric according to any one of claims 1 to 10.

12. The absorbent article according to claim 11, wherein the absorbent article is a disposable diaper, a sanitary napkin or incontinence pad.

* * * * *

Strength Optimization of Thermally Bonded Spunbond Nonwovens

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ABSTRACT

Recent research on all aspects of thermally point bonded nonwovens has led to considerable improvements in the understanding of material requirements for these nonwovens, the changes that occur during bonding and the resultant deterioration of the mechanical properties of the nonwoven materials. This paper addresses how one may use a bicomponent fiber technology to overcome the shortcomings of the thermal bonding and obtain high strength spunbond fabrics. In particular, we present the utility of islands-in-the-sea (I/S) bicomponent fibers for optimizing the strength of thermally bonded fabrics. To examine the role of various bonding temperatures on the fabric performance, pre-consolidated webs were formed and subsequently, thermally bonded. Thus, any influence introduced by potential variations in the structure was minimized. Point-bonded bicomponent samples made up of nylon-6 (N6) as the islands and low density polyethylene (PE) as the sea showed great promise with respect to their mechanical properties, suggesting that the use of bicomponent fibers can be beneficial for strength optimization of thermally bonded spunbond nonwovens.

INTRODUCTION

Thermal calender bonding is one of the most economical and widely used techniques in nonwoven fabric manufacturing [1]. In this process, a pre-consolidated web is passed through the nip of two rolls pressed against each other at a desired pre-set pressure and heated internally to a desired temperature. Often, one of these rolls has an engraved pattern on its surface that leads to fiber-to-fiber bonding locally at the points of the intersection of the engraved pattern with the smooth roll [2]. This type of bonding results in the formation of bonding "points" or "spots" on the fabric and is referred to as point-bonding. Bonding with this technique is achieved by the direct conduction of heat. The nip pressure of the calender brings the fibers together to cause fusion of filaments/fibers at their cross-over

points [2]. Overall, point-bonding is accomplished through three critical steps: 1) heating the web to partially melt the crystalline regions, 2) diffusion of the newly released chain segments across the fiber-fiber interface, and 3) subsequent cooling of the web to cause its re-solidification and to trap the diffused chain segments [3, 4]. The degree of fiber-to-fiber fusion in the bonding spots determines the final strength of the bond and ultimate properties of the fabric.

Many studies have been conducted to determine the optimal conditions for calendering to enhance the performance of bonded fabrics [1-10]. It has been shown that point-bonded spunbond nonwovens are typically not very strong and that bonding temperature at a constant line speed or line speed at a constant bonding temperature has a profound effect on the tensile properties of these fabrics. Typically, with an increase in the bonding temperature or time, the strength of the fabric improves until it reaches a maximum. Any further increase in the temperature or bonding time results in a web lower strength [1-4, 8-9]. At the bonding conditions below the peak, fabric failure occurs by bond disintegration because of insufficient fiber fusion or "under-bonding". At temperatures above the maximum optimal bonding temperature, the failure occurs by fiber breakage at the bond periphery, leaving the bonds intact [1-4, 8, 10]. The fabrics bonded at the high and optimal temperatures are referred to as over-bonded and well-bonded, respectively.

Several explanations of the failure mechanism of over-bonded and well-bonded nonwovens have been provided in literature. One possible cause of such failure mechanism is that the fibers are "crushed" by the calender rolls and thus weakened at the bond edge. However, Chidambaram et al. [5] showed that this factor accounted for only a small portion of the loss of the web strength. Wang et al. [4, 10] studied thermally bonded isotactic polypropylene (iPP) and poly(ethylene terephthalate) (PET) nonwovens and

found a reduction in birefringence (molecular orientation) of the fibers at the bond spot and in its vicinity compared to the original, unbonded fibers. The molecular orientation of the fibers entering the bond spot decreased significantly over a distance of 30-40 microns from the bond edge, implying a large decline in the fiber modulus in this region. The change in the fiber morphology was influenced by bonding conditions and it was significantly smaller in samples bonded at lower temperatures or for shorter times. The properties of bridging fibers at locations greater than 30-40 microns from the bond edge were unchanged from the original fibers. Similar results were observed by Dharmadhikary et al. [6] for PP nonwovens. Chidambaram et al. [5] reported that the large reduction of the fiber birefringence leads to a significant decrease in the fiber strength. Thus, the fibers, having the same diameter along their entire length, are expected to fail where their molecular orientation is the smallest. The birefringence of the fibers is low within the bond and at its edge, but the cross-sectional area of the bond is much larger than that of the fibers, thus the fibers at the bond periphery would fail predominantly [4, 10]. Because the change in the fiber morphology is influenced by bonding conditions, over-bonded webs demonstrate a larger loss of mechanical properties of the fibers entering the bond compared to well-bonded webs [3, 4]. This allows for fabrics bonded at the optimal temperature to show superior mechanical performance over the webs bonded at higher temperatures. Nevertheless, even well-bonded nonwovens demonstrate premature failure at the bond periphery as a result of the partial loss of the fiber strength brought about by the thermal bonding process. It has been hypothesized that if the bridging fibers of well-bonded nonwovens would have the same strength over their entire length, including the region at the bond periphery, it would lead to better load sharing and would potentially result in a stronger web [3].

Our hypothesis is that improved bonding and higher fabric strength could be achieved through the use of bicomponent fibers, such as sheath-core or islands-in-the-sea (I/S) fibers, in which numerous small filaments of one polymer – islands – are placed in a matrix of another polymer – sea. However, the island (core) and sea (sheath) components must have certain characteristics. The island polymer should have higher strength and lower elongation at break than the sea component, and the sea should have a lower melting temperature than the island to allow the bonding of the structure without adversely affecting the islands. Moreover, only in the presence of a strong interface between the island and sea polymers, the mechanical stresses could be transferred between

weak sea and strong islands. If the sea and island materials comply with all previously mentioned requirements, then it is probable that the thermal bonding process would not influence the morphology and the strength of the islands in the vicinity of the bond spots; whereas the sea could be completely melted acting as a binder and transferring the stress to stronger island fibers under the load. This could be a simple way to enhance the properties of the calendered fabrics.

In this paper, we present a study where the effectiveness of the I/S fibers in the optimization of the mechanical performance of thermally bonded spunbond nonwovens was explored.

EXPERIMENTAL

Materials

Ultramid BS 700 nylon-6 (N6) (BASF) was used as the island polymer. The same was also utilized in the production of homo-component fibers and fiber webs. ASPUN 6811A polyethylene (PE) (Dow Chemical Company) and poly (lactic) acid (PLA) (NatureWorks, LLC) were used as the sea. Some of the properties of the polymers are summarized in Table 1.

TABLE 1. Properties of the island and sea polymers

Polymer		Melting Temperature T_m , °C	Density, ρ/cm^3	Specific Heat, $J/kg\cdot K$	B^1 , K
N6	-	220	1.14	1600	6064
-	PLA	173	1.25	1800	9128
-	PE	125	0.94	2200	2727

Keys: ¹Polymer characteristic found experimentally by using inversion procedure and Arrhenius type equation

$\ln \eta_0 = \ln A + (B/T_f)$ where T_f is the polymer

temperature measured in K; η_0 is the polymer zero shear

viscosity measured at T_f ; $B = \frac{E_a}{R}$ where E_a and R are

the polymer activation energy and universal gas constant.

Methods

Sample preparation

Bicomponent and homo-component pre-consolidated spunbond webs were produced at the Nonwovens Cooperative Research Center (NCRC) Partners' Pilot facilities located at North Carolina State University.

TABLE II. Description of the nonwoven sample processing and bonding conditions

Sample Abbreviation	No of Islands	Polymer		Ratio, %		Processing and Bonding Conditions		
		Island	Sea	Island	Sea	Quenching air velocity, m/s	Spinning speed, m/s	Bonding
100 % N6	0	-	N6	-	100	1.7	45.3	C at 170°C - 200 °C
100 % PE	0	-	PE	-	100	1.0	36.6	
100% PLA	0	-	PLA	-	100	0.5	60.0	
108 I/S 25/75 N6/PE	108	N6	PE	25	75	1.7	41.7	C at 125°C - 155 °C
108 I/S 50/50 N6/PE	108	N6	PE	50	50	1.7	41.9	
108 I/S 75/25 N6/PE	108	N6	PE	75	25	1.7	40.0	
108 I/S 75/25 N6/PLA	108	N6	PLA	75	25	1.7	47.4	

Keys: °C - Calendaring.

The fiber processing and bonding conditions are listed in Table 2. All fibers were quenched at the same cooling temperature of 12.8 °C. The extrusion temperatures of the 100% N6, 100% PE, and 100% PLA fibers were 274, 216, and 227 °C, respectively. In the case of 108 I/S N6/PE fibers, N6 and PE were extruded at 266 and 227 °C, respectively. The extrusion temperatures of N6 and PLA polymers composing 108 I/S N6/PLA fibers were 274 and 227°C, respectively. Calender bonding for all samples was conducted at a speed of 10 m/min with a nip pressure of 70 kN/m (400 pounds per linear inch). The basis weight of fabrics was maintained constant at about 0.2 kg/m². Both free-fall (undrawn) and drawn fibers were collected to examine their properties.

Mechanical properties

The tensile properties of the homo-component and bicomponent fibers were examined according to ASTM D3822-01. Twelve specimens of each sample were used to determine an average breaking force and elongation at break.

The tensile properties such as breaking force and elongation at break for all fabrics were determined according to ASTM D5034. Six specimens (100 x 150 mm) of each sample were tested in machine (MD) and cross-machine (CD) directions, respectively. The tear strength of the fabrics was examined according to ASTM D 2261. Five specimens (75 x 200 mm) of each sample were tested in MD and CD, respectively, and their average values of strength were then calculated. All samples were conditioned at 65%±2% relative humidity and temperature of 21±1 °C prior to each test.

Scanning electron microscopy

The bonding spots and fiber failure mechanisms were examined by Scanning Electron Microscopy (SEM).

Scanning electron micrographs were obtained on a Hitachi S-3200N microscope. Before each measurement, the specimens were coated with a layer of AuPd using a Denton Vacuum Sputter Coater.

Thermal analysis

Thermal analysis was carried out to determine the degree of crystallinity of the bicomponent and homo-component fibers by differential scanning calorimetry (DSC) using a PerkinElmer DSC 7 calorimeter. Standard indium sample was used to calibrate the DSC. Fibers weighing 3 to 4 mg were cut into thin pieces and dried overnight at 40 °C. Samples were scanned at a heating rate 20 °C /min between 25 °C and 250 °C.

RESULTS AND DISCUSSION

Prior to detailed investigation of the applicability of the I/S fibers to the strength optimization of the thermally bonded nonwovens, a study was conducted to determine the influence of the island count on the mechanical properties of bicomponent fibers. Our study revealed that the I/S N6/PE fibers consisting of 108 islands displayed the best and the most consistent performance. Therefore, the 108 I/S N6/PE fibers were used further in the strength optimization study.

Fiber properties

Before the discussion of the mechanical properties of the I/S bicomponent spunbond fabrics, the properties of homo-component and bicomponent fibers with different ratios of island and sea polymers were examined.

N6 and PE were selected as the island and sea polymers, respectively, because N6 homo-component fibers had significantly higher tenacity, modulus and lower elongation at break than PE filaments (Table 3). As it was mentioned earlier in the paper, these differences may facilitate transfer of shear and tensile stresses through the weaker sea component to the

stronger internal phase, i.e. to N6, thus enhancing the strength of the N6/PE filaments. However, such stress transfer may be possible only in the presence of a strong interface between the polymers, as it has been shown by various researchers [11-13]. A weak interface would not allow any substantial stress transfer between the matrix (sea) and the island fibers due to debonding of the islands from the sea and sliding of the islands relative to the weaker matrix.

Such sliding typically results in an abrupt drop in the strength as a consequence of low levels of normal stress acting across the interface [11]. Thus, a weak interface would result in the fiber fracture by phase debonding and relatively low fiber strengths. On the other hand, a strong interface typically leads to fiber failure as a result of crack propagation through the weak phase [13].

TABLE III. Properties of the homo- and bicomponent filaments

N ₆ of Islands	Composition	Strain at Break, %	Tenacity, g/den	Initial Modulus, g/den	Diameter, μm	Denier
0	100 % PE	83.8 ($\sigma=6.9$)	1.0 ($\sigma=0.1$)	13.9 ($\sigma=2.01$)	19.3 ($\sigma=2.0$)	2.5 ($\sigma=0.2$)
0	100 % N6	52.9 ($\sigma=6.2$)	7.2 ($\sigma=0.8$)	178.7 ($\sigma=18.2$)	15.7 ($\sigma=1.9$)	2.0 ($\sigma=0.2$)
0	100 % PLA	12.4 ($\sigma=1.3$)	3.9 ($\sigma=0.4$)	154.8 ($\sigma=16.3$)	13.1 ($\sigma=1.3$)	1.5 ($\sigma=0.1$)
108	25/75 N6/PE	10.6 ($\sigma=3.1$)	2.1 ($\sigma=0.5$)	41.97 ($\sigma=4.7$)	17.6 ($\sigma=1.1$)	2.2 ($\sigma=0.3$)
108	50/50 N6/PE	33.5 ($\sigma=5.2$)	2.9 ($\sigma=0.2$)	51.27 ($\sigma=5.3$)	17.2 ($\sigma=1.0$)	2.2 ($\sigma=0.3$)
108	75/25 N6/PE	26.2 ($\sigma=4.3$)	3.6 ($\sigma=0.5$)	78.5 ($\sigma=8.0$)	17.1 ($\sigma=1.6$)	2.3 ($\sigma=0.3$)
108	75/25 N6/PLA	12.4 ($\sigma=0.1$)	3.2 ($\sigma=0.4$)	104.6 ($\sigma=10.7$)	15.2 ($\sigma=1.0$)	1.9 ($\sigma=0.1$)

Finally, the melting temperature of PE was about 95°C lower than that of N6 (Table I). Thus, PE could act as a "binder" for the bicomponent N6/PE spunbond web during calendering, which in turn, could decrease the risk of thermal damaging of the N6 islands and reducing the ultimate fabric strength.

The diameter of the N6/PE bicomponent fibers was in between that of single component N6 and PE fibers (Table 3). According to Lin et al. [14], such observation may be an indication of a similarity in the component drawing behavior and may point out to a strong interface between the components and their sufficient attenuation in the spunbond bicomponent without sliding or debonding of the polymers on their interface. Because we believe that N6/PE fibers had a relatively strong interface and PE demonstrated a higher elongation at break than N6, it is possible that stress would be transferred between the strong N6 islands and weak PE phase during mechanical testing. This could explain the performance of the N6/PE composite fibers, which was better than that of PE, but worse than the performance of N6 homo-component fibers (Table 3). Our hypothesis about the stress transfer between stronger N6 islands and weaker PE sea through a strong interface between the polymers was also confirmed with a help of SEM analysis of the 108 I/S N6/PE fibers fractured in the Instron testing machine (Figure 1). The figure indicates a strong interface between the components of the bicomponent N6/PE fibers.

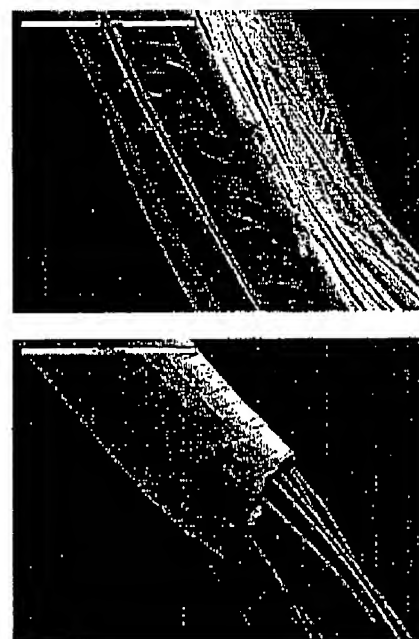


FIGURE 1. 108 I/S 75/25 N6/PE (left) and 108 I/S 75/25 N6/PLA (right) fiber fracture under the load; the scale bars correspond to 50 (left) and 200 (right) microns.

The hypothesis of the stress transfer between island and sea materials can also be illustrated via comparison to other bicomponent filaments, in which the sea had lower elongation at break than the island and the interface between the sea and island was not as strong as in the case of the N6/PE fibers. Table 3 shows that the bicomponent filaments made up of 25% of PLA and 75% of N6 had the tenacity and elongation of nearly pure PLA filaments. This may indicate that the fracture of PLA sea initiated the failure of the bicomponent fiber; or in other words, there was no stress transfer between weak PLA and strong N6 islands due to a weak interface between N6 and PLA polymers and lower elongation at break of the PLA component. Moreover, SEM analysis of the N6/PLA fiber fracture indicated the failure path by mostly debonding in the N6/PLA fibers (Figure 1). Once debonding occurred, the stress transfer between PLA and N6 became impossible.

Our data also showed that the N6/PE filaments with 75% of N6 as the island had the highest values of strength and modulus. Therefore, the composition 75/25 N6/PE was used in our further study.

Homo- and bicomponent substrates – performance at different bonding temperatures

To evaluate the effectiveness of the I/S bicomponent fibers in thermal bonding, the 108 I/S 75/25 N6/PE and 100% N6 pre-consolidated webs were calendered at bonding temperatures ranging from 125 °C to 155 °C and 170 °C to 200 °C, respectively (Table 2). For these series of samples the tongue tear and grab tensile strength values were obtained and plotted as a function of the bonding temperature (Figures 2 and 3).

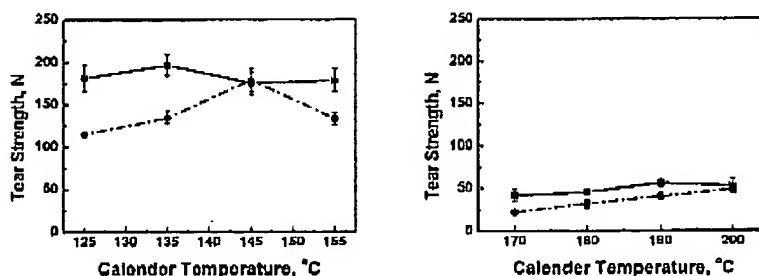


FIGURE 2. Tongue tear strength of the 108 I/S 75/25 N6/PE (left) and N6 (right) sample series as a function of the bonding temperature: solid lines - MD; dash-dot lines - CD.

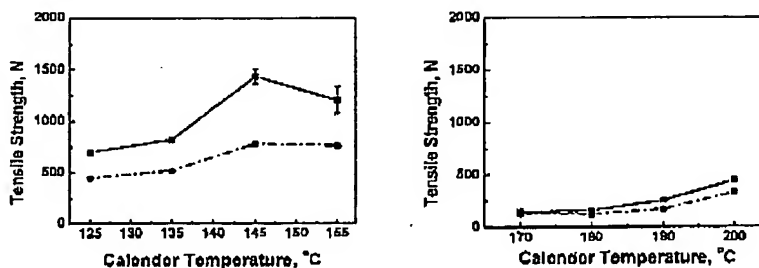


FIGURE 3. Grab tensile strength of the 108 I/S 75/25 N6/PE (left) and N6 (right) sample series as a function of the bonding temperature: solid lines - MD; dash-dot lines - CD.

As can be seen from these figures, the bicomponent fabric bonded at 145 °C and N6 fabric bonded at 200 °C showed the maximum tensile strength in both directions and the highest tear strength only in CD. The MD tongue tear data demonstrated peak values at 135 °C and 190 °C for bicomponent and homo-component sample series, respectively. Because the tensile properties of the bicomponent fabric started to deteriorate after 145 °C, this temperature was

considered to be optimal for bicomponent sample series under the conditions used. The most favorable bonding temperature for the N6 samples was considered to be 200 °C because webs bonded at this temperature demonstrated no delaminating during testing in contrast to other N6 nonwovens bonded at lower temperatures.

Overall, all I/S bicomponent sample series showed considerably better performance than the 100 % N6 homo-component nonwovens. For comparison, the 108 I/S 75/25 N6/PE fabric, bonded at its optimum bonding temperature (145 °C), had a tongue tear strength about three to four times higher than that of the homo-component N6 fabric bonded at 200 °C. The grab tensile strength of the same bicomponent fabric was more than three times higher in the MD and more than two times higher in the CD than the tensile strength of the N6 fabric. These data demonstrate the effectiveness of the I/S bicomponent fibers in improving the performance of these fabrics.

Homo- and bicomponent substrates – difference in the bonding mechanisms

The difference in the bonding mechanisms of homo- and bicomponent fabrics can be seen from the appearance of the fibers in the bond spot and at the bond periphery of these fabrics (*Figures 4 and 5*).

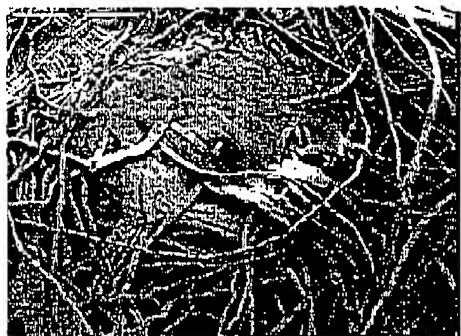


FIGURE 4. Bond spots of 100 % N6 fabric bonded at 200 °C: the scale bar corresponds to 500 microns.

As can be noted from *Figure 4*, the homo-component N6 fibers in the bond spot and its vicinities were damaged; they became flat and also lost their definition. This could mean that N6 fibers within and in the vicinities of the bond spots endured significant macro and micro morphological changes, in comparison to the original, un-bonded fibers, and possibly became weaker due to the loss of their molecular orientation as a result of heat diffusion. Thus, in the presence of the strong thermal bonds, the failure in the calendered fabric is expected to propagate along the weak bridging fibers entering the bond spots, as was reported before [1-4, 8, 10]. If this is true, then the comparison of the performance of the mechanically bonded webs consisting of original, undamaged N6 fibers to a thermally bonded fabric, in

which N6 fibers supposedly lost their strength, would show that the mechanically bonded webs perform significantly better than the thermally bonded ones. To prove the point, three N6 sample series were examined: calendered only, hydroentangled only, and calendered after hydroentangling (*Table 4*). Hydroentangling was chosen because it is a mechanical bonding process, in which the web of loose fibers is entangled by multiple rows of fine, high pressure water jets. Thus, because no fiber melting is involved in this bonding process, hydroentangling should not affect fiber morphology or strength. Indeed, the hydroentangled N6 spunbonded fabrics were stronger than their thermally bonded counterparts and the hydroentangled structures lost their properties after being calendered. This confirms that thermal bonding of homo-component N6 webs causes irreversible morphological changes in the N6 fibers entering the bond spots, leading to a lower performance.



FIGURE 5. Bond spot (left) and the fibers in the bond spot (right) of the 108 I/S 75/25 N6/PE fabric bonded at 145 °C: the scale bars correspond to 500 (left) and 50 (right) microns.

TABLE IV. Tensile and tear strength of the N6 homo-component fabrics

Bonding Method	Tensile Strength, N		Tear Strength, N	
	MD	CD	MD	CD
Calendering at 200 °C	446.4 ($\sigma=20.6$)	328.6 ($\sigma=30.4$)	53.0 ($\sigma=8.8$)	49.1 ($\sigma=3.9$)
1 pass of hydroentangling	758.3 ($\sigma=23.5$)	412.0 ($\sigma=23.5$)	75.5 ($\sigma=2.9$)	87.3 ($\sigma=9.8$)
1 pass of hydroentangling + Calendering at 200 °C	701.4 ($\sigma=30.4$)	362.0 ($\sigma=28.5$)	40.2 ($\sigma=12.8$)	64.8 ($\sigma=2.9$)

In the case of the 108 I/S N6/PE point-bonded fabrics, the N6 islands were enwrapped by the completely molten PE sea, but the fibrous structures of the islands remained intact along their entire length (Figure 5). This could mean that the bonding temperature of 145 °C was too low to cause a significant change in the morphology or the strength of the N6 islands along their entire length, including the region at the bond periphery, which is known to be the weakest link in well-bonded webs [1-4, 8, 10]. At the same time, the temperature of 145 °C caused complete melting of PE sea, leading to formation of solid, unfailing bonds. If strong bonds are formed, then the fabric failure would be expected to occur in the bridging fibers at the bond edge [1-4, 8, 10].

N6 polymer has higher activation energy of elongational viscosity and lower specific heat than PE (Table 1), thus under the same quenching conditions the N6 islands comprising the bicomponent fibers would be expected to solidify earlier in the spunbond spin-line than the PE sea. Therefore, the islands should experience higher elongational stresses than the sea [15-20]. According to Kikurani et al. [16], if one component solidifies while the other is still in a low viscous state, the elongational stress experienced by the latter vanishes instantly and stress relaxation could occur in the second component leading to its molecular orientation relaxation. Hence, during the N6/PE I/S fiber spinning we could expect simultaneous development and suppression of the molecular orientation in the N6 islands and PE sea, respectively. If the PE sea was indeed initially poorly orientated,

then very little loss of its molecular orientation or strength would be expected during the thermal bonding process of the I/S webs [3]. At the same time, because of supposedly intact islands, the strength of the bridging bicomponent fibers, including the region at the bond periphery, in the thermally bonded N6/PE nonwovens should not differ essentially from the strength of the original, unbonded N6/PE I/S fibers. If this is true, then due to the strong thermal bonds formed and intact bridging fibers the thermally bonded bicomponent I/S nonwovens would be expected to perform significantly better than their mechanically bonded counterparts because thermal bonds involve fiber interfusion rather than interlocking and they are typically much stronger than mechanical bonds.

To confirm this hypothesis, three N6/PE sample series were examined — calendered only, hydroentangled only, and calendered after hydroentangling (Table 5). The hydroentanglement produced nonwovens having the lowest values of the tensile and tear strength. These values were comparable to those obtained for the hydroentangled homo-component N6 fabrics with the exception of the tensile strength in MD direction. After being calendered, the 108 I/S 75/25 N6/PE hydroentangled fabrics showed an increase in the tensile and tear properties, unlike N6 hydroentangled webs. However, the highest values of the strength were demonstrated by the nonwovens calendered at optimal temperature of the bonding.

TABLE V. Tensile and tear strength of the 108 I/S 75/25 N6/PE bicomponent fabrics

Bonding Method	Tensile Strength, N		Tear Strength, N	
	MD	CD	MD	CD
Calendering at 145 °C	1435.2 ($\sigma=75.5$)	779.9 ($\sigma=30.4$)	175.6 ($\sigma=13.7$)	178.5 ($\sigma=13.7$)
1 pass of hydroentangling	263.9 ($\sigma=7.9$)	431.6 ($\sigma=10.8$)	71.6 ($\sigma=5.9$)	69.7 ($\sigma=9.8$)
1 pass of hydroentangling + Calendering at 145 °C	1029.1 ($\sigma=38.3$)	570.9 ($\sigma=17.7$)	169.7 ($\sigma=13.7$)	126.6 ($\sigma=2.9$)

These results show that the thermal bonding of the I/S N6/PE structures leads to the improved performance of the calendered spunbonds due to formation of the strong bonds without adversely affecting the bicomponent fiber strength. The data also may be considered as a circumstantial proof of the low degree of molecular orientation developed in PE sea as a result of the bico-spinning of essentially incompatible polymers, such as N6 and PE.

Homo- and bicomponent substrates – crystallinities

To examine the morphological changes in the homo-component and bicomponent fibers after thermal bonding, the 100% N6 and 108 I/S 75/25 N6/PE fibers before and after calendering at the temperatures 200 °C and 145 °C, respectively, were analyzed by using DCS. The results are listed in Table 6.

As may be seen from this Table 6, crystallinity of both 100% N6 and N6/PE I/S fibers, entering the bond spots, reduced after thermal bonding; however, this reduction was insignificant for the components comprising the N6/PE filaments. This, in turn, confirms our previous statements that calendering of N6 homo-component webs caused significant changes in the morphology and thus strength of the bridging fibers at the bond spots. On the other hand, the morphology or strength of the N6/PE bridging fibers, entering the bond spots, in the calendered webs was almost unchanged. Therefore, we believe that the significant loss of the fiber strength at the bond periphery of the thermally bonded N6 webs, in contrast to a little loss of the fiber strength at the bond edge of the N6/PE thermally bonded nonwovens, were responsible for the poor performance of the N6 fabrics in comparison to the performance of the N6/PE sample series.

TABLE VI. Values of the heat of fusion (ΔH) and crystallinity (χ) obtained from the DSC thermograms of the N6 homo-component and N6/PE bicomponent fibers before and after calendering

I/S	Composition	Sample Description	ΔH_{N6} , J/g	ΔH_{PE} , J/g	χ_{N6} , %	χ_{PE} , %
0	100% N6	Fibers before bonding	75.8 ¹	-	32.9 ¹	-
0	100% N6	Bridging fibers at the bond edge after bonding	59.4 ¹	-	25.8 ¹	-
108	75/25 N6/PE	Fibers before bonding	49.8 ²	28.4 ³	21.6 ²	9.7 ³
108	75/25 N6/PE	Bridging fibers at the bond edge after bonding	48.1 ²	23.5 ³	20.9 ²	8.0 ³

Keys: ¹ The heat of fusion and crystallinity of the N6 homo-component fibers; ² The heat of fusion and crystallinity of the N6 island component comprising the N6/PE I/S fibers; ³ The heat of fusion and crystallinity of the PE sea component composing the N6/PE I/S fibers.

Optimization study – polymer ratios and number of islands

Although the results of the mechanical testing of the I/S N6/PE fibers indicated that the fibers made up of 75% of N6 showed the best performance, the

influence of the polymer ratio on the fabric mechanical properties was also investigated. Pre-consolidated spunbond webs made up of fibers with 85%, 75%, and 50 % of N6 were calendered at 145 °C and their mechanical properties were determined (Figure 6).

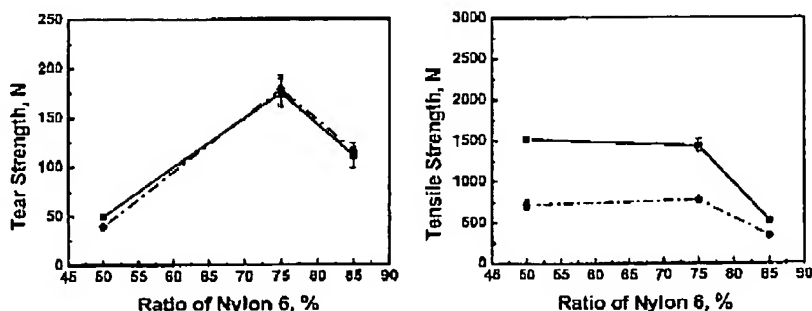


FIGURE 6. Tear (left) and tensile (right) strength of 108 I/S N6/PE fabric as a function of polymer ratios; solid lines - MD; dash-dot lines - CD.

As can be seen from the figure, the fabric containing 75% of N6 had the highest tear strength in both directions and the highest tensile strength in CD. When using nylon ratios higher than 75%, it is

probable that the amount of the sea polymer was not sufficient to completely bind the structure together and consequently, the web properties deteriorated.

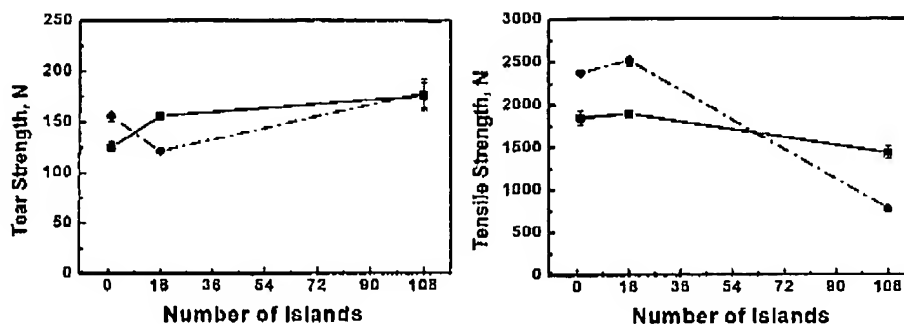


FIGURE 7. Tear (left) and tensile (right) strength of the bicomponent 75/25 N6/PE fabric as a function of the number islands: solid lines - MD; dash-dot lines - CD.

To determine the effect of the number of islands on the mechanical properties of the calendered bicomponent nonwoven fabrics, pre-consolidated spunbond webs made up of fibers with 1, 18, and 108 islands were calendered at 145 °C and tested for their tear and grab tensile strength. The results of the tests are presented in Figure 7. The figure shows that the 18 I/S N6/PE fabric had the highest tensile strength, whereas the 108 I/S N6/PE fabric demonstrated the highest tear strength in both directions. The latter may be explained by the fact that when tear propagates through the 108 I/S N6/PE fabric, a larger number of the islands are released and bunch together, absorbing significant tearing energy. Therefore, the 108 I/S N6/PE webs demonstrated tear performance superior to that of other nonwovens made up of smaller number of islands.

Note, however, that all I/S structures performed significantly better than N6 homocomponent sample series. This confirms again the fact that in contrast to the thermal bonding of 100% N6 webs, calendering of the N6/PE bicomponent structures allowed formation of the strong, unfailing bonds without damaging of the bicomponent fiber strength.

CONCLUSIONS

In this paper, we have demonstrated that by using bicomponent islands-in-the-sea fiber technology it is possible to overcome the shortcomings of the thermal bonding process and produce nonwovens with significantly higher strength. Our study has revealed that the strength of a calendered fabric could be improved significantly with the use of the I/S fibers, such as N6/PE, which have a relatively strong

interface between the polymers and sufficient differences in the properties of the island and sea components. In the N6/PE fibers, the N6 islands had higher strength, modulus, and melting temperature and lower strain at break than the PE sea. The thermal bonding process caused complete melting of the PE sea, leaving the islands intact along their entire length. Moreover, it is possible that the un-oriented and weaker PE phase endured very little, if any, change in the morphology or strength during the thermal bonding process. Therefore, the strength of the bridging bicomponent N6/PE fibers, including the region at the bond periphery, in the thermally bonded nonwovens did not differ from those of the original, un-bonded N6/PE I/S fibers. During mechanical testing, the weaker PE acted as a matrix that held the structure together and helped transfer the stress to the stronger, oriented islands via a strong interface between the sea and islands. This led to the superior performance of the calendered N6/PE fabrics over that of the calendered N6 webs, in which fibers in the bond spots and their vicinities underwent sufficient loss of the molecular orientation or strength. Among different number of islands and polymer ratios, nonwovens containing filaments with 18 and 108 I/S and composed of 75% of N6 and 25% of PE demonstrated the best tensile and tear strength, respectively.

Although calendering of the N6/PE sample series at the temperature of 145 °C seemed to result in the fabrics having superior performance over that of the samples bonded at other temperatures or by other methods, the high strength of the examined nonwovens was achieved at the cost of their

flexibility and permeability. To enhance these properties of the bicomponent fabrics without damaging their strength, other bonding possibilities need to be considered. These include through air thermal bonding, hydroentangling or needlepunching prior calendering or through air bonding, etc.

This paper was focused on the mechanisms and the differences brought about by using the I/S fibers, such as N6/PE, to achieve higher strengths in thermally bonded substrates. Although substantial experiments were conducted, much remains to be done to develop a full and complete understanding of the underlying material-process-property interactions. These include a detailed investigation of the failure mechanism of the thermally bonded I/S fabrics and the study of the influence of various polymer combinations, on the performance of the thermally bonded I/S fabrics. Some of these factors will be addressed in a subsequent paper.

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REFERENCES

- [1] Bhat, G. S., Jangala, P. K. and Spruiell, J. E.; Thermal bonding of polypropylene nonwovens: effects of bonding variables on the structure and properties of the fabrics, *J. Appl. Polym. Sci.*; vol. 92, pp. 3593-3600, 2004.
- [2] Bhat, G. S. and Malkan, S. R.; Extruded continuous filament nonwovens: advances in scientific aspects, *J. Appl. Polym. Sci.*; vol. 83(3), pp. 572-585, 2002.
- [3] Michielsen, S., Pourdeyhyimi, B. and Desai, P.; Review of thermally point-bonded nonwovens: materials, processes, and properties, *J. Appl. Polym. Sci.*; vol. 99(5), pp. 2489-2496, 2006.
- [4] Wang, X. and Michielsen, S.; Morphology gradients in thermally point-bonded poly(ethylene terephthalate) nonwovens, *Textile Res. J.*; vol. 72(5), pp. 394-398, 2002.
- [5] Chidambaram, A., Davis, H. and Baira, S. K.; Strength loss in thermally bonded polypropylene fibers, *Intl. Nonwovens J.*; vol. 9(3), pp. 27-36, 2000.
- [6] Dharmadhikary, R. K. et al.; Influence of fiber structure on properties of thermally point bonded polypropylene nonwovens, *Textile Res. J.*; vol. 69, pp. 725-734, 1999.
- [7] Kim, H. S. et al.; Characterizing structural changes in point-bonded nonwoven fabrics during load-deformation experiments, *Tex. Res. J.*; vol. 71(2), pp. 157-164, 2001.
- [8] Kim, H. S. and et al.; Anisotropy in the mechanical properties of thermally spot-bonded nonwovens: experimental observations, *Tex. Res. J.*; vol. 71(11), pp. 965-976, 2001.
- [9] Kim, H. S. and et al.; Effect of bonding temperature on load-deformation structural changes in point-bonded nonwoven fabrics, *Tex. Res. J.*; vol. 72(7), pp. 645-653, 2002.
- [10] Wang, X. and Michielsen, S.; Morphology gradients in thermally point-bonded polypropylene nonwovens, *Textile Res. J.*; vol. 71(6), pp. 475-480, 2001.
- [11] Li, Z. and et al.; Dynamic fiber debonding and frictional push-outs in the model composite systems: experimental observations, *Experimental Mechanics*; vol. 42 (3), pp. 417-425, 2002.
- [12] Schadler, L. S., Giannaris, S. C. and Ajayan, P. M.; Load transfer in carbon nanotube epoxy composites, *Appl. Phys. Letters*; vol. 73(26), pp. 3842-3844, 1998.
- [13] Stamhuis, J. E.; Mechanical properties and morphology of polypropylene composites. III. Short glass fiber reinforced elastomer modified polypropylene, *Polymer Composites*; vol. 9(4), pp. 280-284, 1988.
- [14] Lin, X. D. and et al.; Study on Poly (ethylene terephthalate)/Polypropylene Microfibrillar composites. II. Solid state drawing behavior, *J. Appl. Polym. Sci.*; vol. 93, pp. 1989-2000, 2004.
- [15] Choi, Y. B. and Kim, S. Y.; Effects of interface on the dynamic mechanical properties of PET/Nylon 6 bicomponent fibers, *J. Appl. Polym. Sci.*; vol. 74, pp. 2083-2093, 1999.

- [16] Kikutani, T. and et al.; High-speed melt spinning of bicomponent fibers; mechanism of fiber structure development in poly(ethylene terephthalate)/Polypropylene system, *J. Appl. Polym. Sci.*; vol. 62, pp. 1913-1924, 1996.
- [17] El-Salmawy, A., Miyamoto, M. and Kimura, Y.; Preparing a core-sheath bicomponent fiber of poly(butylene terephthalate). Poly(butylenes succinate-co-L-lactide), *Tex. Res. J.*; vol. 70(11), pp. 1011-1018, 2000.
- [18] Cho, H. H. and et al.; Fine structure and physical properties of Polyethylene/Poly(ethylene terephthalate) bicomponent fibers in high-speed spinning. I. Polyethylene sheath / Poly(ethylene terephthalate) core fibers, *J. Appl. Polym. Sci.*; vol. 77, pp. 2254-2266, 2000.
- [19] Rwei, S. P., Jue, Z. F. and Chen, F. L.; PBT/PET conjugated fibers: melt spinning, fiber properties and thermal bonding, *Polymer engineering and science*; vol. 44(2), pp. 331-344, 2004.
- [20] Yoshimura, M. and et al.; Structure formation of blend and sheath/core conjugated fibers in high-speed spinning of PET, including a small amount of PMMA, *J. Macromol. Sci.: Part B - Physics*; vol. B42 (2), pp. 325-339, 2003.

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